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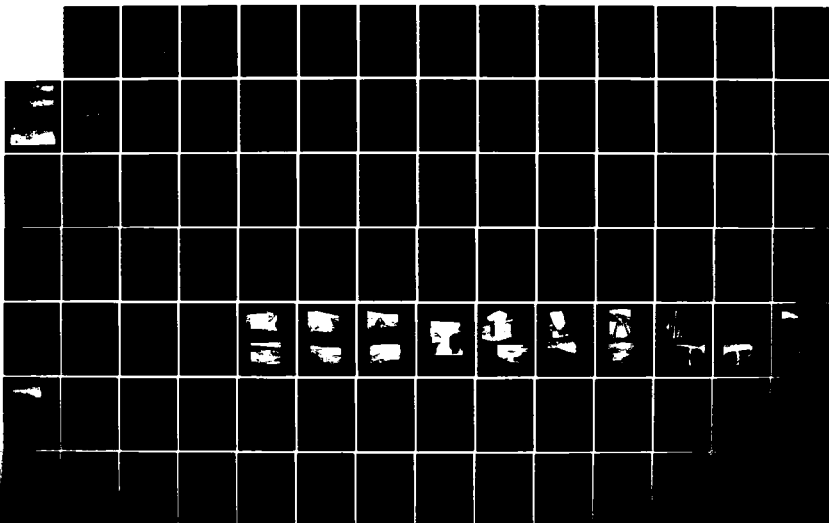
NATIONAL PROGRAM FOR INSPECTION OF NON-FEDERAL DAMS  
BAKER FLOODWATER RESE. (U) CORPS OF ENGINEERS WALTHAM  
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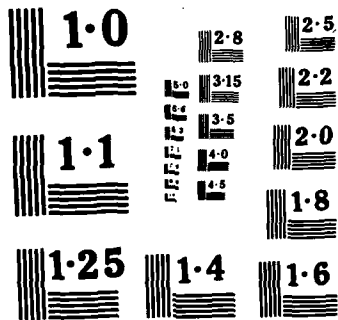
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AD-A156 414

MERRIMACK RIVER BASIN  
DORCHESTER, NEW HAMPSHIRE

**BAKER FLOODWATER RESERVOIR  
SITE 8**

**NH 00178**

NHWRB NO. 66.08

**PHASE I INSPECTION REPORT  
NATIONAL DAM INSPECTION PROGRAM**

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The dam is a 1462 ft. long 62 ft. high earthen structure. The dam is judged to be in good condition. It is intermediate in size with a high hazard potential classification. Debris on the low stage trash rack and separation of the wingwall and training of the outlet works structure were noted during the inspection.		

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DEPARTMENT OF THE ARMY  
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424 TRAPELO ROAD  
WALTHAM, MASSACHUSETTS 02154

REPLY TO  
ATTENTION OF:

NEDED

OCT 2 1979

Honorable Hugh J. Gallen  
Governor of the State of New Hampshire  
State House  
Concord, New Hampshire 03301

Dear Governor Gallen:

I am forwarding to you a copy of the Baker Floodwater Reservoir, Site-8 Phase I Inspection Report, which was prepared under the National Program for Inspection of Non-Federal Dams. This report is presented for your use and is based upon a visual inspection, a review of the past performance and a brief hydrological study of the dam. A brief assessment is included at the beginning of the report. I have approved the report and support the findings and recommendations described in Section 7 and ask that you keep me informed of the actions taken to implement them. This follow-up action is a vitally important part of this program.

A copy of this report has been forwarded to the Water Resources Board, the cooperating agency for the State of New Hampshire. In addition, a copy of the report has also been furnished the owner, New Hampshire Water Resources Board, Concord, New Hampshire 03301.

Copies of this report will be made available to the public, upon request, by this office under the Freedom of Information Act. In the case of this report the release date will be thirty days from the date of this letter.

I wish to take this opportunity to thank you and the Water Resources Board for your cooperation in carrying out this program.

Sincerely,

  
MAX B. SCHEIDER

Colonel, Corps of Engineers  
Division Engineer

Incl  
As stated

BAKER FLOODWATER RESERVOIR SITE 8

NH 00178

NHWRB 66.08

MERRIMACK RIVER BASIN  
DORCHESTER, NEW HAMPSHIRE

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PHASE I INSPECTION REPORT  
NATIONAL DAM INSPECTION PROGRAM



LETTER OF TRANSMITTAL  
FROM THE CORPS OF ENGINEERS TO THE STATE  
TO BE SUPPLIED BY THE CORPS OF ENGINEERS



NATIONAL DAM INSPECTION PROGRAM  
PHASE I - INSPECTION REPORT  
BRIEF ASSESSMENT

Identification No.: 00178  
Name of Dam: Baker Floodwater Reservoir Site 8  
Town: Dorchester  
County and State: Grafton, New Hampshire  
Stream: South Branch Baker River  
Date of Inspection: May 17, 1979

Baker River Floodwater Reservoir Site 8 is a 1,462 foot long 62 foot high earthen structure. There are four different fill zones in the dam including a cutoff wall. Top width of the dam is 14 feet. The upstream and downstream embankments are on a  $2\frac{1}{2}$  horizontal to 1 vertical slope. Appurtenant structures consist of a principal spillway, Saint Anthony's Falls (SAF) type stilling basin and an emergency spillway. The principal spillway has two inlets, a low stage orifice and a high stage, covered top spillway. The inlets discharge through a riser to a 5 foot diameter concrete pipe. There is a 30 inch diameter gated pond drain. The dam construction was completed in September of 1968. Plans, design calculations, and construction data were prepared by the Soil Conservation Service and are available for inspection.

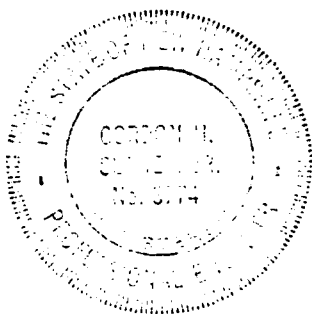
The visual inspection revealed that the dam is in good condition. The inspection revealed the following: surface deterioration of the concrete of the riser structure, debris on the low stage trash rack, and separation of the wingwall and training wall of the outlet works structure.

Based on the intermediate size of the dam and its high hazard classification and in accordance with Corp of Engineers guidelines, the test flood inflow is equal to the Probable Maximum Flood (PMF) or 29,000 cfs. The routed test flood outflow of 20,500 cfs overtops the dam by 0.4 foot. With the water surface at the top of the dam, the spillways will pass 84 percent of the routed test flood outflow. As there is a high hazard to loss of life from large flows downstream a review of the capacity of the spillways for their ability to pass  $\frac{1}{2}$  the PMF was made. The results indicate that the  $\frac{1}{2}$  PMF inflow of 14,500 cfs would result in a routed  $\frac{1}{2}$  PMF

outflow of 7,000 cfs. As the total capacity of the spillways is 17,310 cfs, there will be a freeboard of 2.6 feet. The hydraulic design calculations indicate that the principal spillway was designed for a 100 year frequency flood. The crest elevation of the dam was designed using a total watershed runoff of 10.1 inches.

It is recommended that the owner engage a qualified engineer to investigate the separation of the wingwall and training wall of the outlet works structure and to design modifications to that structure to alleviate the problem. Remedial measures include development of a downstream warning system in the event of emergency conditions, and repair of the deteriorating concrete surface of the riser structure.

The recommendations and remedial measures are described in Section 7 and should be addressed within two years after receipt of this Phase I - Inspection Report by the owner.



*Gordon H. Slaney, Jr.*  
Gordon H. Slaney, Jr., P.E.  
Project Engineer

HOWARD NEEDLES TAMMEN & BERGFENOFF  
Boston, Massachusetts

## PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation and analyses involving topographic mapping, subsurface investigations, testing and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test Flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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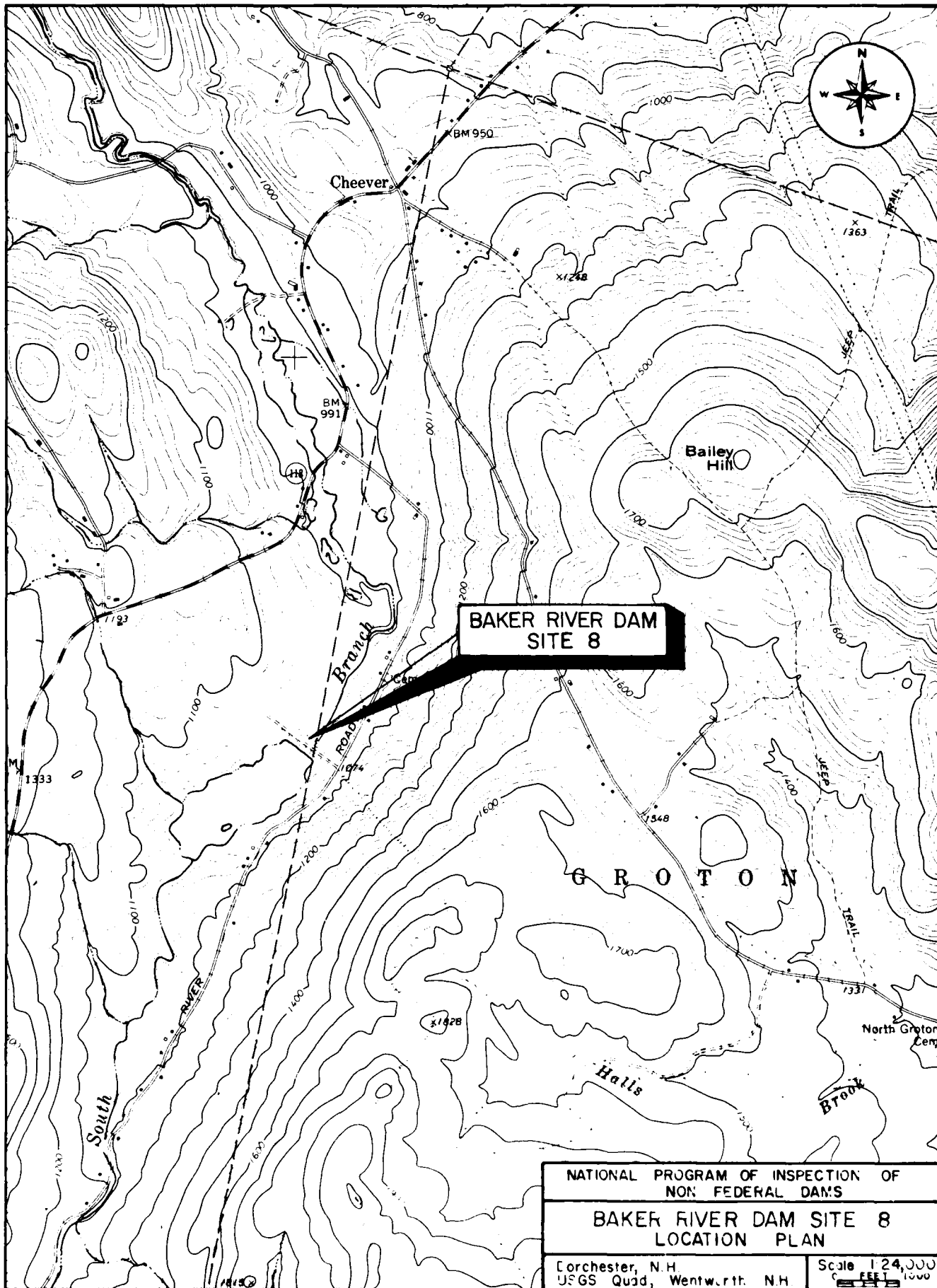
APPENDIX D - HYDROLOGIC AND HYDRAULIC COMPUTATIONS

APPENDIX E - INFORMATION AS CONTAINED IN THE NATIONAL  
INVENTORY OF DAMS



BAKER RIVER DAM SITE 8 - Overview looking upstream

REPRODUCED AT GOVERNMENT EXPENSE



BAKER RIVER DAM  
SITE 8

NATIONAL PROGRAM OF INSPECTION OF NON-FEDERAL DAMS	
BAKER RIVER DAM SITE 8 LOCATION PLAN	
Corchester, N.H. USGS Quad, Wentworth, N.H.	Scale 1:24,000 1 inch = 2,000 feet



NATIONAL DAM INSPECTION PROGRAM  
PHASE I INSPECTION REPORT  
BAKER FLOODWATER RESERVOIR SITE 8

SECTION 1  
PROJECT INFORMATION

1.1 General

a. Authority. Public Law 92-367, August 8, 1972, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a National Program of Dam Inspection throughout the United States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region. Howard, Needles, Tammen & Bergendoff has been retained by the New England Division to inspect and report on selected dams in the State of New Hampshire. Authorization and notice to proceed were issued to Howard, Needles, Tammen & Bergendoff under a letter of March 30, 1979 from John P. Chandler, Colonel, Corps of Engineers. Contract No. DACW33-79-C-0060 has been assigned by the Corps of Engineers for this work.

b. Purpose

(1) To perform technical inspection and evaluation of non-Federal dams to identify conditions which threaten the public safety and thus permit correction in a timely manner by non-Federal interests.

(2) To encourage and prepare the states to initiate quickly effective dam safety programs for non-Federal dams.

(3) To update, verify and complete the National Inventory of Dams.

1.2 Description of Project

a. Location. Baker Floodwater Reservoir Site 8 (Baker Dam Site 8 also known as South Branch Dam) is located on the South Branch Baker River approximately 1 mile upstream from Route 118 in the Town of Dorchester, New Hampshire. The dam is shown on U.S.G.S. Quadrangle Wentworth, New Hampshire, with approximate coordinates N43°46'30", W71°54'54", Grafton County, New Hampshire. The location of Baker Dam Site 8 is shown on the preceding page.

b. Description of Dam and Appurtenances. Baker Dam Site 8 is an earthen embankment structure. Total length of the dam according to existing drawings is 1,462 feet. Maximum structural height is 73 feet, and the height from the top of dam to the streambed is 62 feet. According to the plans there are four different fill zones in the structure, which include a cutoff wall. Top width of the dam is 14 feet. The embankment is on a  $2\frac{1}{2}$  horizontal to 1 vertical slope both up and downstream.

Appurtenant structures consist of a concrete riser and pipe principal spillway with a covered top inlet. There are two stages to the inlet structure, a low stage orifice and a high stage covered inlet. The riser discharges through a 5.0 foot diameter concrete pipe and Saint Anthony's Falls (SAF) Type stilling basin. The emergency spillway is located on the left side of the dam and has a width of 400 feet. It is an excavated earthen structure with a vegetative cover. A 30 inch diameter pond drain can be operated from the riser structure to drain the pond by a 30 inch gate valve.

Figures 1 and 2, located in Appendix B, show a plan of the dam and appurtenant structures. Photographs of each structure are shown in Appendix C.

c. Size Classification. Intermediate (hydraulic height - 62 feet, storage - 4,784 acre-feet) classification based on height being between 40 and 100 feet and storage being between 1,000 acre-feet and 50,000 acre-feet as given in Recommended Guidelines for Safety Inspection of Dams.

d. Hazard Classification. The potential for hazard posed by this dam is classified as high. Failure of the dam at maximum pool elevation (top of dam) would probably result in a total flood wave averaging approximately 20 feet high through the reach studied. About 8 dwellings would probably be inundated and two major roads would be affected.

e. Ownership. This dam is owned by the New Hampshire Water Resources Board, 37 Pleasant Street, Concord, New Hampshire.

f. Operator. This dam is maintained and operated by the New Hampshire Water Resources Board. Chairman of the Water Resources Board is Mr. George McGee, Sr.; Mr. Vernon Knowlton is Chief Engineer, Telephone No. 603/271-1110.

g. Purpose of Dam. This dam is used for floodwater control. The normal pool is maintained by the low stage intake in the riser. The storage between the low stage outlet and the emergency spillway crest is used to retard flood flows of up to a 100 year frequency.

h. Design and Construction History. The construction of this dam was completed in September of 1968. Design and construction inspection of this dam were done by the Soil Conservation Service, Durham, New Hampshire. The construction contractor was Landers and Griffin, Inc., Portsmouth, New Hampshire. In 1977, drain fill was added to the fill behind the wingwalls immediately downstream of the SAF stilling basin.

i. Normal Operating Procedures. The normal pool is maintained by the low stage inlet on the riser. Under flood conditions, when the capacity of the low stage orifice is exceeded, the storage is utilized. The high stage outlet will reach maximum design discharge before the reservoir reaches the crest of the emergency spillway. The dam does not require any manual operation in order to function.

### 1.3 Pertinent Data

a. Drainage Area. The area tributary to Baker Dam Site 8 consists of 16.04 square miles of wooded, mountainous terrain. There is little upstream development. Maximum elevation in the watershed is 2,564 feet MSL. The design flood pool elevation is 1,060.2 feet.

The shoreline and banks of the reservoir are clear of trees. However, the land surrounding this area is heavily wooded and mountainous. There are no cottages, docks or recreational facilities on the reservoir.

#### b. Discharge at Dam Site

(1) Outlet works for Baker Dam Site 8 consist of an emergency spillway, a riser with a low stage orifice and a high stage covered top spillway, and a 30 inch pond drain pipe controlled by a 30 inch gate valve. Invert of the pond drain is at 1,012.0 feet. Maximum discharge of the pipe when the reservoir is at the normal pool level of 1,023.0 feet is about 91 cfs. The low stage orifice has two openings each 36 inch by 17 inches in size set at invert 1,023.0. Capacity of the low stage inlet when the reservoir is at the crest of high stage inlet (1,050.0 ft.) is 236 cfs. The high stage covered inlet crest set at elevation 1,050.0 feet has a capacity of 628 cfs when the water level is at the emergency spillway crest of 1,064.5 feet. The 400 foot wide emergency spillway has a crest at elevation of 1,064.5 feet. When the water surface is at the top of dam (elevation 1,070.5) the spillway will have a capacity of 16,560 cfs.

(2) There are no records available of maximum discharge at the site. However, during the inspection of the dam on May 17, 1979, it was noted that debris on the face of the dam reached to about elevation 1,040.4 which would correspond to a discharge of about 190 cfs.

(3) The spillway and riser capacity with the water surface at the top of the dam is approximately 17,310 cfs at elevation 1,070.5.

(4) Spillway and riser capacity with the water surface elevation at the test flood elevation of 1,070.9 feet is approximately 19,360 cfs.

(5) The total project discharge at the test flood elevation of 1,070.9 feet is 20,500 cfs.

c. Elevation (feet above MSL)

- (1) Streambed at centerline of dam - 1,007.5.
- (2) Maximum tailwater - unknown.
- (3) Upstream portal invert pond drain - 1,012.0.
- (4) Normal pool - 1,023.0.
- (5) Full flood control pool - 1,060.2.
- (6) Spillway crest (emergency spillway) - 1,064.5.  
(riser crest) - 1,050.0.
- (7) Design surcharge - 1,060.2.
- (8) Top Dam - 1,070.5.
- (9) Test Flood Surcharge - 1,070.9.

d. Reservoir (miles)

- (1) Length of Maximum Pool - 1.23.
- (2) Length of Normal Pool - 0.5.
- (3) Length of Flood Control Pool - 1.14.

e. Storage (gross acre-feet)

- (1) Normal Pool - 143.0.

- (2) Flood Control Pool - 3,150.
- (3) Emergency Spillway Crest - 3,760.
- (4) Top Dam - 4,784.

f. Reservoir Surface (acres)

- (1) Normal Pool - 30.
- (2) Flood Control Pool - 140.
- (3) Emergency Spillway Crest - 161.
- (4) Test Flood Pool - 177.
- (5) Top Dam - 177.

g. Dam

- (1) Type - earth.
- (2) Length - 1,462 feet.
- (3) Height - 62 feet hydraulic  
73 feet structural
- (4) Top Width - 14 feet.
- (5) Side Slopes - 2½ horizontal to 1 vertical  
up and downstream.
- (6) Zoning - 4 zones of fill.
- (7) Impervious core - none.
- (8) Cutoff - zone 1 fill.
- (9) Grout Curtain - none.
- (10) Other - none.

h. Diversion and Regulating Tunnel

See Section j below.

i. Principal Spillway

- (1) Type - Concrete Riser Covered Top - 60 inch diameter  
discharge pipe through dam.

- (2) Length of Weir - 30 feet total.
- (3) Crest Elevation - 1,050.0.
- (4) Gates - none.
- (5) U/S Channel - none.

Emergency Spillway

- (1) Type-Earth, overflow
- (2) Length of Weir - 400 feet
- (3) Crest Elevation - 1,064.5
- (4) Gates - none
- (5) U/S Channel - Approach channel from reservoir is 400 feet wide with 4:1 side slopes.

(6) Downstream Channel. Immediately downstream of the dam a channel was constructed for a distance of 350 feet and lined with riprap on the bottom and sides. The natural channel downstream is about 20 feet wide. There are trees on both sides of the channel. Erosion due to high flows was vident along the banks.

j. Regulating Outlets. The normal level of the reservoir is controlled by two 36 inch by 17 inch orifice inlets set in the riser at invert elevation 1,023.0. There is a trash rack for each opening but no control gates. The 30 inch pond drain pipe set at invert 1,012.0 extends 176 feet into the reserovir from the riser and has a trash rack at the intake. The pipe is controlled at the riser by a 30 inch gate valve.

## SECTION 2 ENGINEERING DATA

### 2.1 Design

A complete set of design data including layout, hydraulic design, foundation and embankment design, geology and soils reports, structural design, quantities and specifications are available for Baker Dam Site 8. In addition, there are construction drawings available. Design of the dam was done by the Soil Conservation Service, Durham, New Hampshire.

### 2.2 Construction

The dam construction was completed in September of 1968. A complete record of construction documents were made available. These documents include as-built plans, job diaries, surveying records, test drilling logs, compaction test results, concrete tests and certificate of completion. Construction was by Landers and Griffin, Inc., Portsmouth, New Hampshire, and was inspected by the soil conservation Service, Durham, New Hampshire.

In 1977, drain fill was added behind the wingwalls at the downstream end of the discharge channel.

### 2.3 Operation

Normally, the pond drain line gate is closed. The normal level of 1,023.0 is maintained by the low stage orifice openings. The principal spillway riser and reservoir storage is designed to retard runoff from up to a 100 year frequency storm without discharge occurring in the emergency spillway (crest 1,064.5).

### 2.4 Evaluation

a. Availability. Engineering data available for Baker Dam Site 8 consists of the information outlined in Sections 2.1 and 2.2. The plans, design data and construction records are available at the offices of the Soil Conservation Service, Federal Building, Durham, New Hampshire 03824.

b. Adequacy. A complete set of design and construction data did allow for a definitive review within the confines of this Phase I - Inspection Report. Therefore, the adequacy

of this dam is based on the design and construction data reviewed, visual inspection, past performance history and sound engineering judgment.

c. Validity. The field investigation indicated that the external features of Baker Dam Site 8 substantially agree with those shown on the available plans.



SECTION 3  
VISUAL INSPECTION

3.1 Findings

a. General. The field inspection of Baker Dam Site 8 was made on May 17, 1979. The inspection team consisted of personnel from Howard, Needles, Tammen & Bergendoff and Geotechnical Engineers, Inc. A representative of the New Hampshire Water Resources Board was also present during the inspection. Inspection checklists, completed during the inspection, are included in Appendix A. At the time of inspection the water level was 0.4 feet above the invert of the low stage intake. The upstream face of the dam could only be inspected above this water level.

b. Dam. Visual inspection indicates the dam is in excellent condition.

The dam is an earth embankment 1,462 feet long and 62 feet high. The embankment consists of a wide upstream zone of sand and silty sand and a downstream zone of poorly-graded gravel. A cutoff trench extends below the central portion of the dam. There is a trench drain and blanket drain beneath the downstream section of the dam.

An unpaved emergency spillway has been cut into the left abutment and an outlet works consisting of a drop inlet structure, a concrete conduit through the dam and an outlet structure is located near the right abutment.

Upstream Slope

The upstream slope is 2.5 horizontal to 1 vertical. Reservoir storage was such that the entire upstream slope was inspected. The slope is well turfed and in good condition, as shown in Photo No. 3.

Crest

The crest of dam is 14 feet wide and is grass covered with grass with the exception of an unpaved roadway which is shown in Photo No. 5. No significant misalignment of the crest was observed.

Downstream Slope

The downstream slope is 2.5 horizontal to 1 vertical. The slope shown in Photos No. 4 and 6 is grass covered and in good condition.

No seepage or damp areas were observed along the toe of the dam.

The dam has a trench drain and blanket drain which exit the discharge channel just below the stilling basin. At the time of inspection, these drain pipes were clear and dry.

c. Appurtenant Structure. Visual inspection of the concrete riser spillway structure, emergency spillway and outlet works structure did not reveal any evidence of stability problems. The riser structure generally appeared to be in good condition, except for surface deterioration in the form of staining, cracks and scaling, Photos No. 7, 8, 9 and 10. The spillway trash racks and service ladder are in good condition. No rust or peeling of the protective coating were noted.

The concrete riser structure (principal spillway) consists of three elements: An overflow control with a low stage inlet and a high stage crest, a vertical transition and a closed discharge conduit. The riser structure is placed in the embankment. Visual inspection revealed that the riser structure appeared to be in good condition, except for water staining, cracks and extensive surface scaling in the form of loss of surface mortar and in some locations loss of coarse aggregate particles.

The 30 inch diameter pond drain pipe, intake and gate could not be inspected as they were under water. The gate and control mechanism are housed in the concrete riser tower. The control mechanism appeared to be in good condition.

The trash racks at the low and high flow control stages consist of a standard shape angles and grating. Both trash rack assemblies are in good condition. No rust or peeling of the protective coating was noted. The low stage trash rack structure is filled with debris.

The emergency spillway is a grass covered excavation in the left abutment passing around the dam. The spillway is shown in Photos No. 18, 19 and 20.

The earth spillway is in good condition. The channel downstream of the emergency spillway is heavily wooded.

The outlet works structure at the toe of earth dam consists of 60 inch reinforced concrete pipe and Saint Anthony's Falls Type stilling basin structure with u-type training walls and wingwalls, see Photos No. 12 and 13.

Visual inspection of the outlet works structure reveals that the concrete surface is generally in good condition except for the wingwalls which have moved approximately 2.5 inches from the training walls. The movement is horizontal (sliding) as seen in Photos No. 14, 15, 16 and 17 causing a cutting of the plastic waterstops. There appears to be no rotational movement. The movement of the wingwalls does not pose a safety problem to the dam.

The discharge channel below the stilling basin extends for a distance of 350 feet downstream of the outlet works (Photo No. 12). The channel is lined with rock riprap and is in excellent condition.

d. Reservoir Area. The reservoir area is in mountainous terrain. The shoreline is clear of trees. There are no cottages, docks or recreational facilities on the reservoir. Debris was noted on the upstream face of the dam.

e. Downstream Channel. The stream regains the natural channel downstream of the riprap lined outlet channel. The natural channel is about 20 feet wide and both banks are lined with trees. Some debris was noted in the channel. The banks show some signs of erosion due to high flows.

### 3.2 Evaluation

Visual examination indicates generally the dam is in good condition. The inspection revealed the following:

(a) Some surface deterioration in the form of staining, cracking and scaling of the concrete on the riser portion of the principal spillway.

(b) Debris on the low stage trash rack.

(c) Separation of the wingwalls and training walls of the outlet works structure due to movement (sliding) of the wingwalls.

## SECTION 4 OPERATIONAL PROCEDURES

### 4.1 Procedure

Baker Dam Site 8 is used for floodwater control. Under normal operating procedures, the dam is left to function as designed. The normal pool level is maintained by the low stage orifice openings in the riser. Flood events of up to a 100 year frequency are retarded by the reservoir storage between the normal pool and the emergency spillway crest. The emergency spillway is utilized only with events greater than a 100 year frequency.

### 4.2 Maintenance of Dam

The dam is inspected on an annual basis by the New Hampshire Water Resources Board and the Soil Conservation Service. Maintenance is undertaken as a result of the inspection on an as needed basis. The dam is visited on a monthly basis by personnel of the Water Resources Board.

### 4.3 Maintenance of Operating Facilities

Maintenance of the outlet works is performed as in Section 4.2.

### 4.4 Description of Warning Systems

There are no warning systems in effect for this facility.

### 4.5 Evaluation

The current operation and maintenance procedures for this facility appear to be adequate to insure that any problems encountered can be remedied within a reasonable period of time. However, the owner should establish a downstream warning system to follow in the event of emergency conditions.

SECTION 5  
HYDROLOGY AND HYDRAULIC ANALYSIS

5.1 Evaluation of Features

a. General. Baker Dam Site 8 is an earthen embankment dam 1,462 feet long with a hydraulic height of 62 feet. The dam is constructed with four fill zones and a earth fill core. Appurtenant works consist of two stage riser and 5.0 foot diameter concrete pipe which discharges to a Saint Anthony's Falls type stilling basin, an emergency spillway 400 feet wide and a 30 inch diameter gated pond drain.

The dam is used for floodwater control. The dam is classified as intermediate in size having a height of 62 feet and maximum storage of 4,784 acre-feet.

b. Design Data. According to the Soil Conservation Service design data, this dam is constructed to retard flood flows of up to a 100 year frequency storm without utilizing the emergency spillway. The design flood control elevation is 1,060.2 feet or 4.3 feet below the emergency spillway crest. Total runoff for this condition is 3.62 inches during a six hour Type IIB storm. The crest elevation of the dam was designed using a total watershed runoff of 10.10 inches. The structure is classified as having a "C" hazard which is defined as "dams located where failure may cause loss of life, serious damage to homes, industrial and commercial buildings, important public utilities, main highways or railroads.

c. Experience Data. There are no records available of maximum discharge at the dam site. However, during the inspection of the dam on May 17, 1979, it was noted that debris on the face of the dam reached to about elevation 1,040.4 which would correspond to a discharge of about 190 cfs.

d. Visual Observations. No evidence of damage to any portion of the project from overtopping was visible at the time of inspection.

e. Test Flood Analysis. Even though detailed design and operational data are available for this dam, a hydrologic evaluation was performed using a test flood equal to the Probable Maximum Flood (PMF) as determined from Guide Curves issued by the Corps of Engineers. Based on a drainage area of 16.04 square miles, it was estimated that the test flood inflow at Baker Dam Site 8 would be 29,000 cfs. Following the guidance for Estimating Effect of Surcharge Storage on Maximum Probable Discharge results in a routed test flood outflow discharge of 20,500 cfs. As the maximum capacity

of the spillways at the top of dam is 17,310 cfs (approximately 84 percent of the routed test flood outflow), the test flood will result in the dam being overtopped by approximately 0.4 feet. The test flood was routed with the water surface starting at the normal pool elevation.

As there is a high hazard to loss of life from large flows downstream of the dam (resulting from dam failure), and dam failure resulting from overtopping would significantly increase the hazard to loss of life downstream from the dam, a review of the spillway capacity for its ability to pass  $\frac{1}{2}$  the PMF was made. This analysis indicates that the test flood inflow would be approximately 14,500 cfs. Following the guidance for Estimating Effect of Surcharge Storage on Maximum Probable Discharge results in a routed  $\frac{1}{2}$  PMF outflow of 7,000 cfs. As the total capacity of the spillways at the top of dam is 17,310 cfs, the spillway can safely pass the routed  $\frac{1}{2}$  PMF outflow with a free board of approximately 2.6 feet.

f. Dam Failure Analysis. The impact of failure of the dam at maximum pool (top of dam) was assessed using the "Rule of Thumb" Guidance for Estimating Downstream Hazard Hydrographs issued by the Corps of Engineers. The analysis covered the reach extending from the dam to a point 5.5 miles downstream at the intersection of Route 25 and 118 with the South Branch Baker River. The downstream channel stage, prior to breach of dam, with the spillway discharging at full capacity, will be 3 feet above the river bank or about 8 feet from the streambed. After breach, the total flood wave height of 25 feet at the dam will be reduced to about a 17 foot height by the end of the reach studied. About 8 dwellings along this reach will probably be inundated. Two major roads, Route 118, one mile downstream of the dam and Route 25, 5.5 miles downstream will be affected by the floodwave.

SECTION 6  
STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

a. Visual Observation. The visual inspection did not disclose any immediate stability problems. Although some movement of the wingwall on the outlet works was observed, it did not pose a problem to the safety of the dam.

b. Design and Construction Data

Design drawings and construction specifications exist and indicate the dam is a zoned embankment consisting of a wide upstream zone of silty sand, sand and a downstream zone of poorly-graded gravel. A cutoff trench extends below the central portion of the dam. The cutoff trench extends up both abutments, but its depth could not be determined from the available drawings.

A Drainage trench and blanket drain are located beneath the downstream zone of the embankment.

A grass-covered emergency spillway passes around the embankment on the left abutment.

Construction records indicate that the dam and appurtenant structures were built according to the plans and specifications.

A review of the design calculations and drawings was made in order to determine the cause of movement of the wingwalls at the outlet works. The movement is horizontal. There appears to be no rotational movement, probably because the end of wingwall is embedded in the riprap placed below the wall to shape the discharge channel.

The wingwalls were designed as cantilever walls, expansion joints with water-stop were placed between the training walls and cantilever wingwalls.

c. Operating Records. No operating records are available.

d. Post Construction Changes. The outlet pipes of the foundation drainage system originally passed immediately behind the outlet works training walls and exited through the wingwalls, as shown in Photo No. 13. In 1977, in order to provide better drainage around the SAF outlet, the location of the drain pipes was moved away from the outlet works and carried below the structure to outlet into the discharge channel. The new drain pipe

outlets were below the water surface at the time of inspection. The work included plugging of the old drain pipes, placement of new drain fill material around the relocated drain pipe and placement of the  $\frac{1}{4}$  inch thick plates behind each separation of the training wall and wingwall. All modifications were designed by the Soil Conservation Service.

Piezometers were installed behind each wingwall in 1973 as part of the investigation to remedy the wall movement. The study was conducted by professional engineers from the New Hampshire State SCS office in conjunction with professional engineers from the regional SCS office in Bromall, Pennsylvania. The above noted modifications are based on recommendations from this study. The report entitled "Report on Investigation of Structural Deficiency - Site 8, Baker River Watershed - Grafton County, New Hampshire," dated March 1976 is available on request from the SCS. The piezometer pipes may be seen in Photo No. 12.

e. Seismic Stability. The dam is located in Seismic Zone 2 and in accordance with the recommended Phase I guidelines does not warrant seismic analysis.



SECTION 7  
ASSESSMENT, RECOMMENDATION AND REMEDIAL MEASURES

7.1 Dam Assessment

a. Condition. The visual inspection of Baker Floodwater Reservoir Site 8 indicates the dam is in good condition. The inspection revealed the following:

- (1) Some surface deterioration in the form of staining, cracking and scaling of the concrete on the riser portion of the principal spillway.
- (2) Debris in the low stage trash rack.
- (3) Separation of the wingwalls and training walls of the outlet works structure due to movement (sliding of the wingwalls).

The hydraulic analysis reveals that the spillways cannot pass the routed test flood outflow without overtopping the dam.

b. Adequacy. A complete set of design and construction data did allow for a definitive review within the confines of this Phase I - Inspection Report. Therefore, the adequacy of this dam is based on the design and construction data reviewed, visual inspection, past performance history and sound engineering judgment.

c. Urgency. This dam is in generally good condition. The recommendations and remedial measures described in Sections 7.2 and 7.3 should be accomplished within 2 years of the receipt of this Phase I - Inspection Report by the owner.

d. Necessity for Additional Information. No additional investigation is needed to complete the Phase I inspection.

7.2 Recommendations

There are no recommendations resulting from the Phase Inspection.

7.3 Remedial Measures

(a) Clear the debris from the trash rack on the low stage inlet.

(b) Repair the deteriorating surface of the concrete on the riser structure.

(c) Develop a downstream warning system to follow in the event of emergency conditions.

(d) Continue to monitor water levels behind the outlet structure wingwalls and the rate (if any) of further separation.

(e) Continue the periodic inspections on a biennial basis.

(f) The installation of a more permanent type fencing around the outlet works should be considered.

#### 7.4 Alternatives

There are no practical alternatives to the recommendations of Section 7.2 and 7.3.

APPENDIX A  
INSPECTION CHECKLIST



## PERIODIC INSPECTION CHECK LIST

A-2

PROJECT Baker Site No. 8 DamDATE May 17, 1979PROJECT FEATURE Earth EmbankmentNAME D. P. LaGattaDISCIPLINE Geotechnical EngineerNAME C. E. Osgood

AREA EVALUATED	CONDITION
<u>DAM EMBANKMENT</u>	
Crest Elevation	1070.5
Current Pool Elevation	1023.4
Maximum Impoundment to Date	1040.00 estimated from debris level.
Surface Cracks	None observed.
Pavement Condition	No pavement. Grass cover with wheel tracks.
Movement or Settlement of Crest	None observed.
Lateral Movement	None observed.
Vertical Alignment	No misalignment observed.
Horizontal Alignment	No misalignment observed.
Condition at Abutment and at Concrete Structures	Good except for joint separation of wing walls from training walls at principal spillway outlet.
Indications of Movement of Structural Items on Slopes	None.
Trespassing on Slopes	No damage due to trespassers.
Sloughing or Erosion of Slopes or Abutments	Minor surface erosion at a high water-line at an elevation about 15 ft. above the pool.
Rock Slope Protection - Riprap Failures	No riprap on slopes.
Unusual Movement or Cracking at or near Toes	None observed.
Unusual Embankment or Downstream Seepage	None observed.
Piping or Boils	None observed.
Foundation Drainage Features	12" foundation drain outlets are dry and clearn.
Toe Drains	None apparent
Instrumentation System	Measurement points at joints between wing wall and training wall. Piezometer tubes noted at 6 ft. from wingwalls.
Vegetation	Grass cover in good condition.

## PERIODIC INSPECTION CHECK LIST

A-3

PROJECT Site 8, Baker DamDATE May 17, 1979PROJECT FEATURE Intake Channel/StructureNAME D. LaGatta, C. OsgoodDISCIPLINE Geotechnical/Structural EngineersNAME S. Mazur

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - INTAKE CHANNEL AND INTAKE STRUCTURE</u>	
a. Approach Channel	No intake channel.
Slope Conditions	
Bottom Conditions	
Rock Slides or Falls	
Log Boom	None.
Debris	Low trash rack at riser structure is filled with debris.
Condition of Concrete Lining	
Drains or Weep Holes	
b. Intake Structure	Galvanized trash rack and concrete surface of riser structure at both high and low stages of spillway are in good condition. Bottom water release structure (outlet works) was under water. Trash racks need cleaning.
Condition of Concrete	
Stop Logs and Slots	

## PERIODIC INSPECTION CHECK LIST

A-4

PROJECT Site 8, Backer DamDATE May 17, 1979PROJECT FEATURE Control TowerNAME G. SlaneyDISCIPLINE Structural/Hydraulic EngineersNAME S. Mazur

AREA EVALUATED	CONDITION
<p data-bbox="89 449 551 483"><u>OUTLET WORKS - CONTROL TOWER</u></p> <p data-bbox="89 512 535 546">a. Concrete and Structural</p> <p data-bbox="188 575 469 609">General Condition</p> <p data-bbox="188 638 502 672">Condition of Joints</p> <p data-bbox="188 701 328 735">Spalling</p> <p data-bbox="188 764 502 798">Visible Reinforcing</p> <p data-bbox="188 827 700 861">Rusting or Staining of Concrete</p> <p data-bbox="188 890 650 924">Any Seepage or Efflorescence</p> <p data-bbox="188 953 444 987">Joint Alignment</p> <p data-bbox="188 1016 716 1079">Unusual Seepage or Leaks in Gate Chamber</p> <p data-bbox="188 1108 303 1142">Cracks</p> <p data-bbox="188 1171 667 1205">Rusting or Corrosion of Steel</p> <p data-bbox="89 1234 568 1268">b. Mechanical and Electrical</p> <p data-bbox="188 1297 353 1331">Air Vents</p> <p data-bbox="188 1360 386 1394">Float Wells</p> <p data-bbox="188 1423 386 1457">Crane Hoist</p> <p data-bbox="188 1486 337 1520">Elevator</p> <p data-bbox="188 1549 469 1583">Hydraulic System</p> <p data-bbox="188 1612 419 1646">Service Gates</p> <p data-bbox="188 1675 452 1709">Emergency Gates</p> <p data-bbox="188 1738 642 1772">Lightning Protection System</p> <p data-bbox="188 1801 568 1835">Emergency Power System</p> <p data-bbox="188 1864 626 1898">Wiring and Lighting System</p>	<p data-bbox="794 512 1394 722">Outlet works (bottom water release structure) consist of inlet structure and 30" ID reinforced concrete pipe extended to riser structure. Bottom, water release structure including mechanically operated gate were under water.</p> <p data-bbox="794 1247 1402 1436">Mechanically operated gate and control mechanism are housed in concrete riser structure. Gate is operated from roof of riser structure. Gate and control mechanism appear to be in good operational condition.</p>

## PERIODIC INSPECTION CHECK LIST

A-5

PROJECT Site 8, Baker DamDATE May 17, 1979PROJECT FEATURE Spillway/Outlet Works ConduitNAME G. SlaneyDISCIPLINE Structural/Hydraulic EngineersNAME S. Mazur

## AREA EVALUATED

## CONDITION

OUTLET WORKS - TRANSITION AND CONDUIT

General Condition of Concrete

Rust or Staining on Concrete

Spalling

Erosion or Cavitation

Cracking

Alignment of Monoliths

Alignment of Joints

Numbering of Monoliths

At the time of inspection, outlet works conduits were under water. Outlet conduit, dam section, consists of 60" ID reinforced concrete pipe and is placed on concrete bedding. Outlet works, conduit appears to be in good condition.



## PERIODIC INSPECTION CHECK LIST

A-6

PROJECT Site 8, Baker DamDATE May 17, 1979PROJECT FEATURE Outlet Structure/ChannelNAME D. LaGatta, C. OsgoodDISCIPLINE Structural/Hydraulic/GeotechnicalNAME S. Mazur, G. Slaney

AREA EVALUATED	CONDITION
<u>OUTLET WORKS - OUTLET STRUCTURE AND OUTLET CHANNEL</u>	Concrete discharge pipe, stilling basin and training walls are generally in good condition, except that concrete wingwalls are completely separated from training walls at expansion joints (2½" or more).
General Condition of Concrete	
Rust or Staining	Water staining, training and wingwalls.
Spalling	
Erosion or Cavitation	None observed.
Visible Reinforcing	None.
Any Seepage or Efflorescence	None.
Condition at Joints	Expansion joints at wingwalls, 22" opening along training wall; plastic water stop is cut at center of joint, as can be seen in photos N/0 15 & 17
Drain Holes	
Channel	
Loose Rock or Trees Overhanging Channel	Riprap in good condition None
Condition of Discharge Channel	Good, channel clear.

## PERIODIC INSPECTION CHECK LIST

A-7

PROJECT Site 8, Baker DamDATE May 17, 1979PROJECT FEATURE Outlet Works - SpillwayNAME D. LaGatta, C. OsgoodDISCIPLINE Structural/Hydraulic/GeotechnicalNAME S. Mazur, G. Slaney

## AREA EVALUATED

## CONDITION

OUTLET WORKS - SPILLWAY WEIR, APPROACH  
AND DISCHARGE CHANNELS

## a. Approach Channel

General Condition

Good

Loose Rock Overhanging Channel

None

Trees Overhanging Channel

None

Floor of Approach Channel

Grass cover. A few bushes should be mowed. Area damp at time of inspection at left of channel. Poses no threat to dam. This facility has two spillway structures; concrete riser or shaft spillway and auxiliary earth spillway located in left abutment. Both spillways are in good condition.

## b. Weir and Training Walls

General Condition of Concrete

Water staining, cracks and loss of mortar in concrete surface. Photo No. 7

Rust or Staining

None

Spalling

None

Any Visible Reinforcing

None

Any Seepage or Efflorescence

Drain Holes

## c. Discharge Channel

General Condition

Good

Loose Rock Overhanging Channel

None

Trees Overhanging Channel

None

Floor of Channel

Grass covered

Other Obstructions

None

# PERIODIC INSPECTION CHECK LIST

A-8

PROJECT Site 8, Baker Dam

DATE May 17, 1979

PROJECT FEATURE Service Bridge

NAME \_\_\_\_\_

DISCIPLINE \_\_\_\_\_

NAME \_\_\_\_\_

AREA EVALUATED	CONDITION
<p><u>OUTLET WORKS - SERVICE BRIDGE</u></p> <p>a. Super Structure</p> <p>Bearings</p> <p>Anchor Bolts</p> <p>Bridge Seat</p> <p>Longitudinal Members</p> <p>Under Side of Deck</p> <p>Secondary Bracing</p> <p>Deck</p> <p>Drainage System</p> <p>Railings</p> <p>Expansion Joints</p> <p>Paint</p> <p>b. Abutment &amp; Piers</p> <p>General Condition of Concrete</p> <p>Alignment of Abutment</p> <p>Approach to Bridge</p> <p>Condition of Seat &amp; Backwall</p>	<p>This facility has no service bridge.</p>

APPENDIX B

ENGINEERING DATA

1. LIST OF DESIGN, CONSTRUCTION AND MAINTENANCE RECORDS
2. PAST INSPECTION REPORTS
3. PLAN AND DETAILS

AVAILABLE ENGINEERING DATA

1. A set of drawings (36 sheets), dated October 1965, showing plans and details of the dam and appurtenant structures, and another set of drawings (5 sheets), dated April 1976, showing changes to the outlet works structure.
2. Design Data including layout, hydraulic design, geology and soils reports, structural design, quantities and specifications.
3. Construction Data: including as-built plans, job diaries, surveying records, test drilling logs, compaction test results, concrete tests and certificate of completion.

All of the above are on file with the U.S.D.A. Soil Conservation Service, Federal Building, Durham, New Hampshire 03824.

PAST INSPECTION REPORTS

# MAINTENANCE CHECKLIST FOR PL 566 FLOOD CONTROL STRUCTURES

This maintenance checklist is a guide for determining the maintenance required for Public Law 566 flood control structures in New Hampshire. It doesn't take the place of experience and judgment and is not inclusive. Items of a difficult nature to check, such as principal spillway conduit condition, are not included. Intensive checks of these items are necessary at proper intervals. Review of as-built drawings, the design folder, structure history, and previous maintenance reports should be part of the inspection. Prompt maintenance is a vital part of safe and effective operation.

Except where otherwise indicated, completion of this form may be facilitated by ranking maintenance items on a 1 to 4 basis where

- 1 = satisfactory
- 2 = satisfactory, but check carefully at next inspection
- 3 = requires maintenance this season
- 4 = requires immediate attention.

WATERSHED Baker SITE 8 DATE 6-13-78  
 INSPECTED BY Gary Kerr, Lvall Milligan (WRB); Mike Dannehy, Nick Luhtala, Ray Wenninger  
 (SES)

## 1. GENERAL ITEMS

Access Road.	.	.	.	.	.	.	.	.	.	N/A
Site Fencing.	.	.	.	.	.	.	.	.	.	(3)
Traffic Conditions.	.	.	.	.	.	.	.	.	.	1
Vandalism Control.	.	.	.	.	.	.	.	.	.	(3)
Trash Control.	.	.	.	.	.	.	.	.	.	1

COMMENTS Fence at dam continues to be vandalized. SAF should be fenced in  
for safety. Riser has holes in downstream end wall. Probably due to  
bullet impact.

## 2. RESERVOIR

Timber stand at reservoir.	.	.	.	.	.	.	.	.	.	1
Debris and slash.	.	.	.	.	.	.	.	.	.	3
Sediment level in relation to low stage inlet	.	.	.	.	.	.	.	.	.	1

COMMENTS A lot of debris at riser should be removed.

### 3. EMBANKMENT AND EXCAVATED SLOPES

(Report riprap and vegetation and erosion condition under Items 4 and 5.)

	Dam	Dike	Emergency Spillways <sup>1/</sup>		Other	
			left	right	( )	( )
Sliding or sloughing	<u>1</u>	—	<u>1</u>	—	—	—
Holes (rodent and other)	<u>1</u>	—	<u>1</u>	—	—	—
(check especially at embankments)						
Excessive settlement (embankments)	<u>1</u>	—	—	—	—	—
Cracks						
Traverse	<u>1</u>	—	<u>1</u>	—	—	—
Longitudinal	<u>1</u>	—	<u>1</u>	—	—	—
Seepage <sup>2/</sup>	<u>1</u>	—	<u>1</u>	—	—	—
Piping <sup>2/</sup>	<u>1</u>	—	<u>1</u>	—	—	—

COMMENTS \_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

### 4. RIPRAP

	Displ. of Rock	Loss of Spalls	Loss of Bedding	Erosion of Found.	Break- down of Rock
Dam					
Upstream berm	—	—	—	—	—
Principal Spillway Outlet	<u>1</u>	<u>1</u>	<u>1</u>	<u>1</u>	<u>1</u>
Embankment Gutters					
left	—	—	—	—	—
right	—	—	—	—	—
Emergency Spillway					
location _____	—	—	—	—	—
location _____	—	—	—	—	—
Waterways					
location _____	—	—	—	—	—
location _____	—	—	—	—	—
Outlet Channel	<u>1</u>	<u>1</u>	<u>1</u>	<u>1</u>	<u>1</u>
Other _____	—	—	—	—	—

COMMENTS \_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

<sup>1/</sup>Looking downstream.

<sup>2/</sup>Check especially at downstream face of embankments.



5. VEGETATION

	Dam	Emergency Spillways <sup>1/</sup>		Dike	Outlet Channel	Water way	Other ( )
Condition of stand (including need for lime and fertilizer)	—	—	—	—	—	—	—
Undesirable vegetation	—	4	4	—	—	—	—
Drainage (surface)	—	—	—	—	—	—	—
Erosion <sup>2/</sup>	—	—	—	—	—	—	—
Sedimentation	—	—	—	—	—	—	—
Condition of planting	—	—	—	—	—	—	—
Pest control	—	—	—	—	—	—	—
Fire control	—	—	—	—	—	—	—

COMMENTS Brush coming in very heavy on emergency spillway and dam. Needs  
immediate attention. Rest of vegetation looks good.

6. EMBANKMENT, STRUCTURAL, & OTHER DRAINS

		Dam <sup>1/</sup>		Other	
		left	right	( )	( )
Depth of Flow <u>Submerged</u>	With any obstruction	—	—	—	—
(in inches above invert)	Without any obstruction	—	—	—	—
Turbidity of Discharge	With any obstruction	—	—	—	—
(yes, no)	Without any obstruction	—	—	—	—
Condition of Protective	Outside	—	—	—	—
Coating	Inside	—	—	—	—
Obstruction in Flow		—	—	—	—
(yes, no)		—	—	—	—
Animal Guard Condition		—	—	—	—
Outlet Condition		—	—	—	—
Retarding Pool Elevation (ft. msl)	_____ or _____ (ft.)			above	
Other _____	3 or 4 feet above L.S.			below	

COMMENTS \_\_\_\_\_

<sup>1/</sup>Looking downstream.

<sup>2/</sup>Including wave, surface, stream, manmade, and livestock erosion.

7. RISER

Caution Be extremely careful when using ladders. Check condition before using. Ladders are sometimes broken, loose, corroded, and or slippery. Use safety harness.

Ladders:  
~~inside~~ out

Condition of protective coating 1 ;  
Corrosion 1 ; Damaged parts     ; Loose     ;  
Other     .

Concrete:  
~~inside~~ out

Cracking 1 ; Spalling 1 ; Other deterioration 3 ;  
Excessive movement (check joint at riser and conduit)     ; Other     .

Trashracks:  
low and high stage

Condition of protective coatings 1 ; Corrosion 1 ;  
Damaged parts 1 ; Condition of fastenings     ;  
Need of gratings due to beaver     ; Safety condition (protruding fastenings, sharp edges, etc.)     ; Other     .

Manhole:

Condition of protective coatings     ; Corrosion     ;  
Damage     ; Lock operable     ; Other     .

Gate:  
including lifting device, stem; guides, disc

Condition of protective coating     ; Corrosion     ;  
Damaged parts     ; Condition of fastenings     ;  
Stem alignment     ; Lubrication     ; Operation     ; Other     .

Safety Items:

Condition of warning signs     ; Condition of safety equipment     ; Other     .

COMMENTS Outside downstream end of riser has surface holes (bullet maybe)

Steel not exposed. Difficult to see L.S. trash rack well. Did not go  
down riser. Recommend checking riser interior, gate operation, and conduit  
at suitable intervals.

(specify) SAF

Cracking 3; Spalling 1; Other deterioration  
      ; Excessive movement (check joints)       ;  
 Waterstops ; Joint sealant ; Other .

Condition of protective coatings\_\_\_; Corrosion\_\_\_; Damaged parts\_\_\_; Condition of fastenings\_\_\_; Need of gratings due to beaver\_\_\_; Safety condition (protruding fastenings, sharp edges, etc.) ; Other .

Condition of protective coating\_\_\_; Corrosion\_\_\_; Damaged parts\_\_\_; Condition of fastenings\_\_\_; Stem alignment\_\_\_; Operation\_\_\_; Lubrication ; Wood decay ; Other .

Report under "Embankment and Other Drains"

Condition of protective coating\_\_\_; Corrosion\_\_\_; Damaged parts\_\_\_; Condition of Fastenings\_\_\_; Wood decay\_\_\_; Safety condition (protruding fastenings, sharp edges, etc.)\_\_\_; Other .

Condition of warning signs\_\_\_; Condition of  
safety equipment ; Other .

COMMENTS Top of SAF wall cracks should be sealed with flexible caulking or coating (not changed from before, however) to prevent further cracking by freezing.

Stream obstructions.	.	.	.	.	.	.	.	.	.	1
Debris in stream.	.	.	.	.	.	.	.	.	.	1
Sediment bars controlled.	.	.	.	.	.	.	.	.	.	1
Plunge pool stability.	.	.	.	.	.	.	.	.	.	_____
Fish habitat appurtenances	.	.	.	.	.	.	.	.	.	_____
Riprap -- Report under "Riprap" (item 4)										

## COMMENTS

# MAINTENANCE CHECKLIST FOR FL 566 FLOOD CONTROL STRUCTURES

This maintenance checklist is a guide for determining the maintenance required for Public Law 566 flood control structures in New Hampshire. It doesn't take the place of experience and judgment and is not inclusive. Items of a difficult nature to check, such as principal spillway conduit condition, are not included. Intensive checks of these items are necessary at proper intervals. Review of built drawings, the design folder, structure history, and previous maintenance reports should be part of the inspection. Prompt maintenance is a vital part of safe and effective operation.

Except where otherwise indicated, completion of this form may be facilitated by ranking maintenance items on a 1 to 4 basis where

- 1 = satisfactory
- 2 = satisfactory, but check carefully at next inspection
- 3 = requires maintenance this season
- 4 = requires immediate attention.

WATERSHED BAKER RIVER SITE 4 DATE 5-20-77  
 INSPECTED BY KERIC DANNIEH LUNTA  
MILLIAN KELSEY MCDONALD

## 1. GENERAL ITEMS

Access Road.	.	.	.	.	.	.	.	.	1
Site Fencing.	.	.	.	.	.	.	.	.	2
Traffic Conditions.	.	.	.	.	.	.	.	.	2
Vandalism Control.	.	.	.	.	.	.	.	.	2
Trash Control.	.	.	.	.	.	.	.	.	3

COMMENTS REMOVED TRASH FROM UPSTREAM EASE OF  
DAM. LOW STAGE TRASH BARS. ROCK MARKS  
ON RISE PROBABLY FROM GULCHES.

## RESERVOIR

Timber stand at reservoir.	.	.	.	.	.	.	.	.	1
Debris and slash.	.	.	.	.	.	.	.	.	2
Sediment level in relation to low stage inlet	.	.	.	.	.	.	.	.	

COMMENTS CONSIDERABLE AMOUNT OF DEBRIS  
CAUGHT IN <sup>WOODEN</sup> BARS UPSTREAM RIGHT SIDE  
OF RISE

# EMBANKMENT AND EXCAVATED SLOPES

(Report riprap and vegetation and erosion condition under Items 4 and 5.)

	Dam	Dike	Emergency Spillways		Other	
			left	right	( )	( )
Sliding or sloughing	<u>2</u>	—	<u>1</u>	—	—	—
Holes (rodent and other) (check especially at embankments)	<u>1</u>	—	<u>1</u>	—	—	—
Excessive settlement (embankments)	<u>1</u>	—	<u>1</u>	—	—	—
Cracks						
Traverse	<u>1</u>	—	<u>1</u>	—	—	—
Longitudinal	<u>1</u>	—	<u>1</u>	—	—	—
Seepage <u>2/</u>	<u>1</u>	—	<u>1</u>	—	—	—
Piping <u>2/</u>	<u>1</u>	—	<u>1</u>	—	—	—

COMMENTS SOME GROUTING BY ICE ON UPSTREAM SLOPE. ALSO  
SOME PILLING & EROSION. 2 SMALL AREAS OF  
SLUGHING ON DOWNSTREAM FACE OF DAM. THESE  
AREAS ABOUT 150 FT FROM RT. END OF DAM.

## 4. RIPRAP

	Displ. of Rock	Loss of Spalls	Loss of Bedding	Erosion of Found.	Break- down of Rock
Dam					
Upstream berm	—	—	—	—	—
Principal Spillway Outlet	—	—	—	—	—
Embankment Gutters					
left	—	—	—	—	—
right	—	—	—	—	—
Emergency Spillway					
location	—	—	—	—	—
location	—	—	—	—	—
Waterways					
location	—	—	—	—	—
location	—	—	—	—	—
Outlet Channel	<u>1</u>	<u>1</u>	<u>1</u>	<u>1</u>	<u>1</u>
Other <u>SAF OUTLET LT. SIDE</u>	<u>1</u>	<u>1</u>	<u>1</u>	<u>1</u>	<u>1</u>

COMMENTS CONTRACTOR WORKING ON RT SIDE OF  
SAF OUTLET

Looking downstream.

2/Check especially at downstream face of embankments.

VEGETATION

	Dam	Emergency Spillways <sup>1/</sup>		Dike	Outlet Channel	Water way	Other ( )
		left	right				
Condition of stand (including need for lime and fertilizer)	<u>3</u>	<u>2</u>	—	—	<u>NA</u>	—	—
Undesirable vegetation	<u>3</u>	<u>2</u>	—	—	<u>3</u>	—	—
Drainage (surface)	<u>NA</u>	<u>1</u>	—	—	<u>NA</u>	—	—
Erosion <sup>2/</sup>	<u>3</u>	<u>1</u>	—	—	<u>1</u>	—	—
Sedimentation	<u>1</u>	<u>1</u>	—	—	<u>1</u>	—	—
Condition of planting	<u>NA</u>	<u>NA</u>	—	—	<u>NA</u>	—	—
Pest control	—	—	—	—	—	—	—
Fire control	—	—	—	—	—	—	—

COMMENTS WEST OF DAM NEEDS VEGETATIVE ESTABLISHMENT  
BUSHES GROWING ON DAM FACES. POND JAP IN E.M.  
SPILLWAY RELATIVE TO OTHER SITES. TREEFALL FODDING,  
SMOOTH GRASS SPREADING ON E.M. SPILLWAY. CROWN  
NETCH COMING IN ON DAM.

6. EMBANKMENT, STRUCTURAL, & OTHER DRAINS

		Dam <sup>1/</sup>		Other	
		left	right	( )	( )
Depth of Flow	With any obstruction	<u>2</u>	<u>1/4</u>	—	—
(in inches above invert)	Without any obstruction	<u>—</u>	<u>—</u>	—	—
Turbidity of Discharge	With any obstruction	<u>NA</u>	<u>NA</u>	—	—
(yes, no)	Without any obstruction	<u>—</u>	<u>—</u>	—	—
Condition of Protective	Outside	<u>1</u>	<u>1</u>	—	—
Coating	Inside	<u>1</u>	<u>1</u>	—	—
Obstruction in Flow		<u>YES</u>	<u>YES</u>	—	—
(yes, no)					
Animal Guard Condition		<u>0</u>	<u>1</u>	—	—
Outlet Condition		<u>1</u>	<u>1</u>	—	—
Retarding Pool Elevation (ft. msl)	_____ or _____ (ft.)	above below _____			
Other	_____				

COMMENTS LEFT PIPE HALF SUBMERGED AT OUTLET  
IRON ALGAE IN OUTLET OF RT. PIPE

<sup>1/</sup> Looking downstream.

<sup>2/</sup> Including wave, surface, stream, manmade, and livestock erosion.

RISER

Caution Be extremely careful when using ladders. Check condition before using. Ladders are sometimes broken, loose, corroded, and or slippery.  
Use safety harness.

Ladders:  
inside and out

Condition of protective coating\_\_\_;  
Corrosion\_\_\_; Damaged parts\_\_\_; Loose\_\_\_;  
Other\_\_\_.

Concrete:  
inside and out

Cracking\_\_\_; Spalling 2; Other deterioration 2; Excessive movement (check joint at riser and conduit)\_\_\_; Other\_\_\_.

Trashracks:  
low and high stage

Condition of protective coatings\_\_\_; Corrosion\_\_\_; Damaged parts\_\_\_; Condition of fastenings\_\_\_; Need of gratings due to beaver\_\_\_; Safety condition (protruding fastenings, sharp edges, etc.)\_\_\_; Other\_\_\_.

Manhole:

Condition of protective coatings\_\_\_; Corrosion\_\_\_; Damage\_\_\_; Lock operable\_\_\_; Other\_\_\_.

Gate:  
including lifting  
device, stem, guides,  
disc

Condition of protective coating\_\_\_; Corrosion\_\_\_; Damaged parts\_\_\_; Condition of fastenings\_\_\_; Stem alignment\_\_\_; Lubrication\_\_\_; Operation\_\_\_; Other\_\_\_.

Safety Items:

Condition of warning signs\_\_\_; Condition of safety equipment\_\_\_; Other\_\_\_.

COMMENTS WDR PERSONNEL WILL CHECK RISER 2 APPAR-  
TENANCES AT LATER DATE. RISER BACK MARKED  
WITH WHAT APPEARS TO BE BULLET HOLES. THE  
BACK RUB COATING IS SPALLING.

COMMENTS \_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

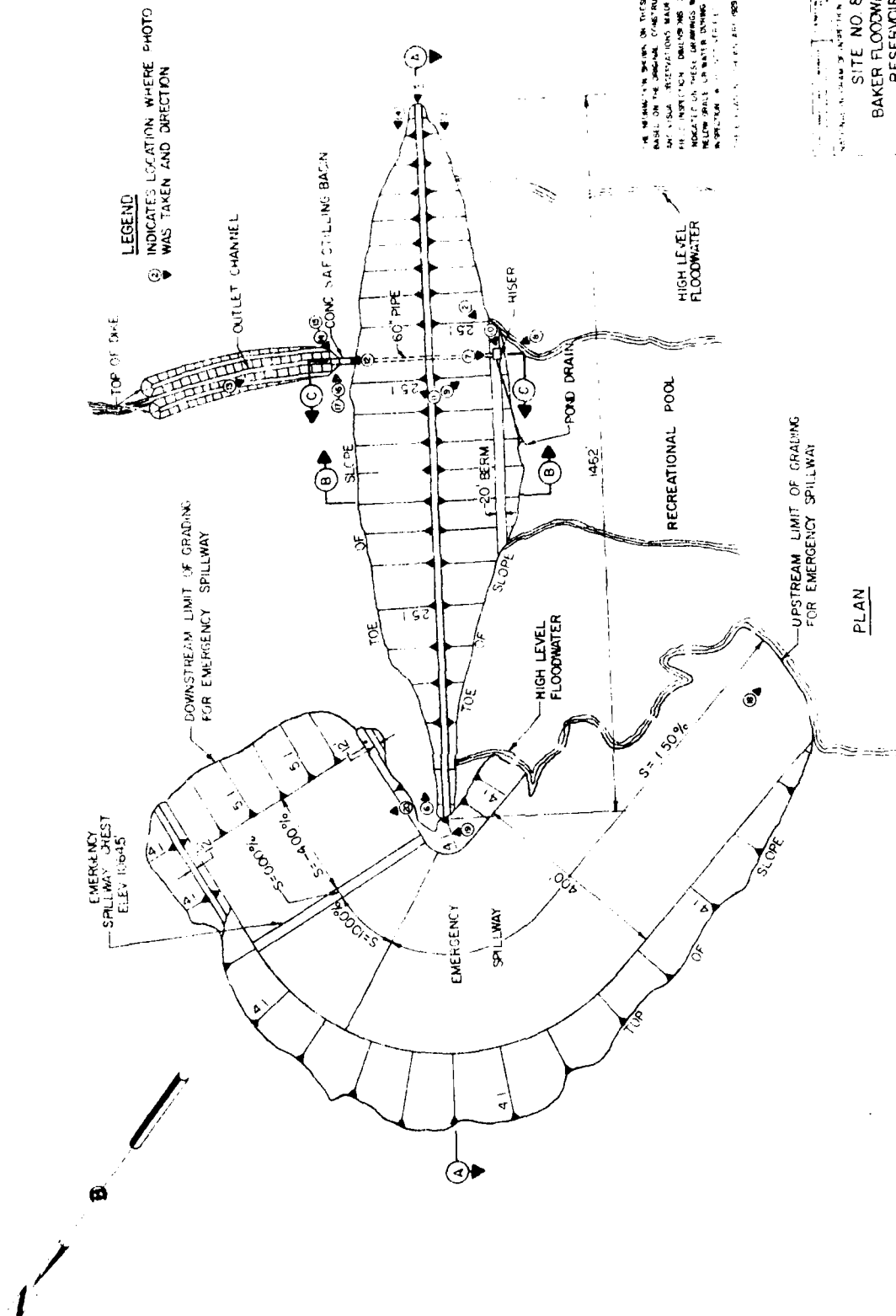




ST. 3-5 K. W. L. 11/21/23

SITE NO. 8  
BAKER FLOODWATER  
RESERVOIR

Fig. 10.2



PLAN



APPENDIX C

PHOTOGRAPHS

FOR LOCATION OF PHOTOS, SEE FIGURE 1  
LOCATED IN APPENDIX B

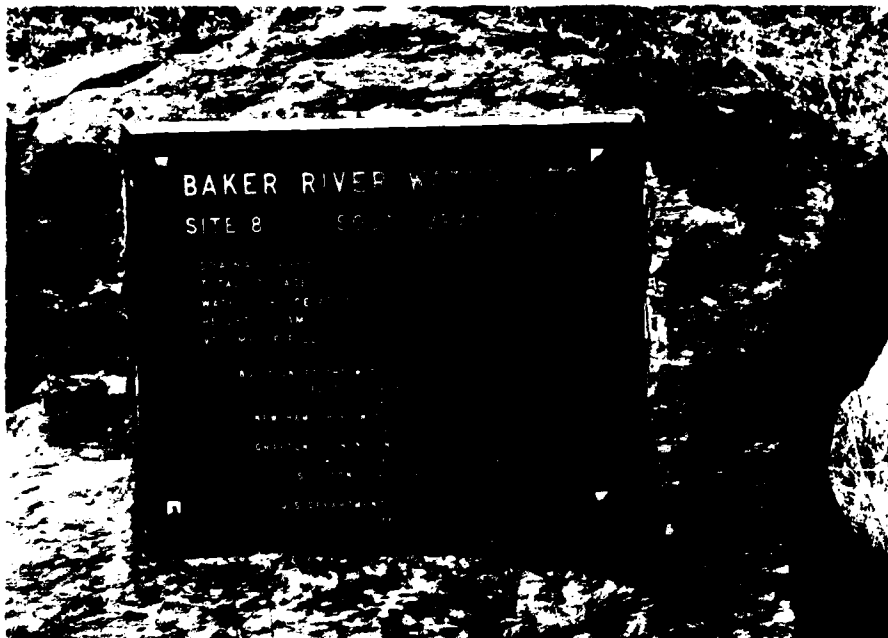


PHOTO NO. 1 - Information monument.



PHOTO NO. 2 - View of principal spillway, riser and portion of reservoir.



PHOTO NO. 3 - View of upstream face of dam from right abutment.



PHOTO NO. 4 - View of downstream slope from right abutment.



PHOTO NO. 5 - View of dam crest from right abutment.

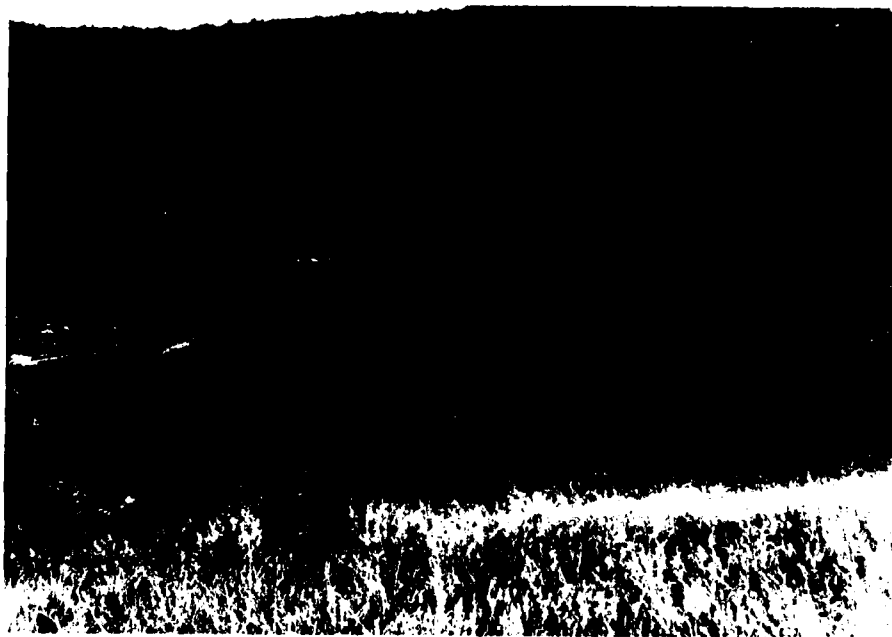


PHOTO NO. 6 - View of downstream slope of dam from left abutment.



PHOTO NO. 7 - View of riser and covered top high stage inlet from dam.





PHOTO NO. 8 - View of  
upstream and right  
side of riser, and  
principal spillway.



PHOTO NO. 9 - View of  
downstream and left  
side of principal  
spillway from crest  
of dam.

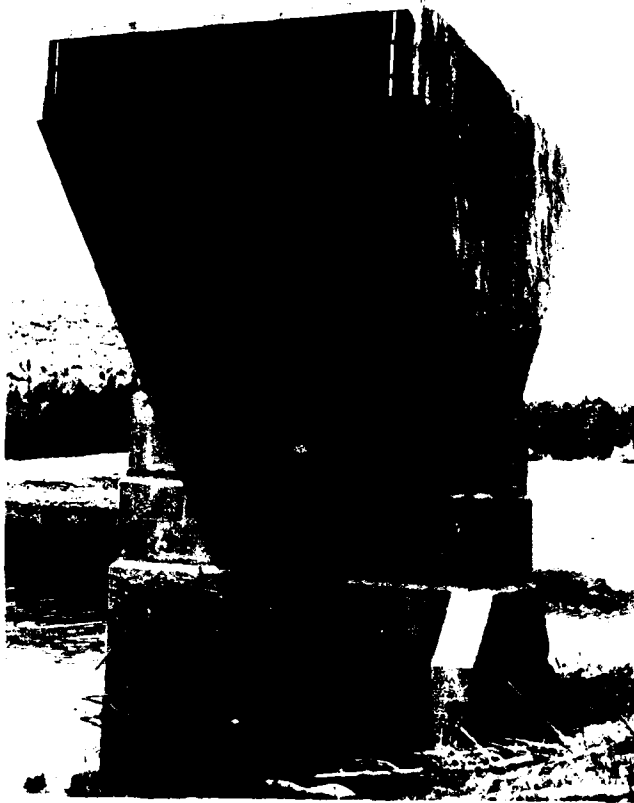


PHOTO NO. 10 - View of  
high stage and low  
stage trash racks on  
right side of prin-  
cipal spillway.



PHOTO NO. 11 - View of outlet works and downstream channel  
from dam.



PHOTO NO. 12 - View of  
a portion of SAF  
stilling basin and  
outlet channel.

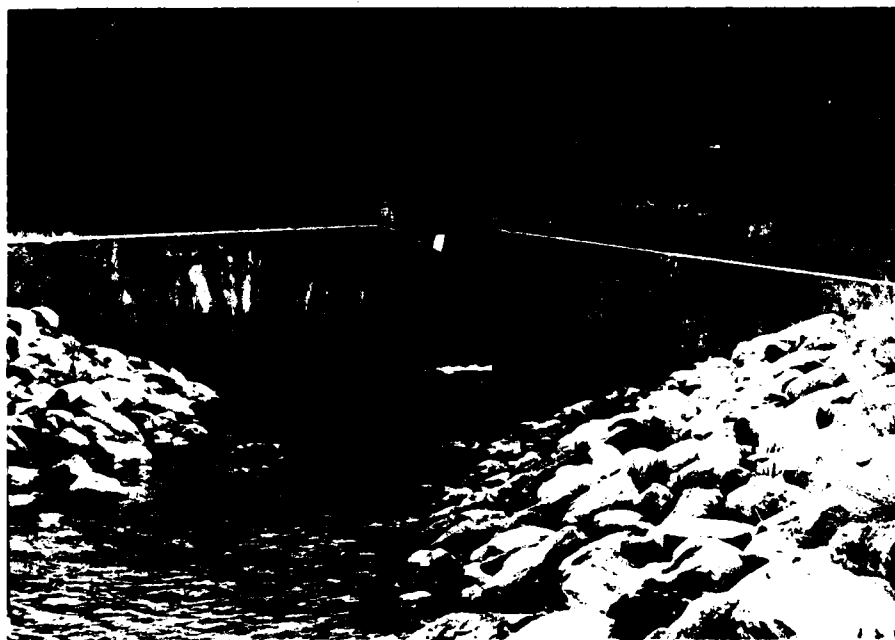


PHOTO NO. 13 - View of outlet works.



PHOTO NO. 14 - View of  
separation between  
right training wall  
and wingwall of out-  
let works.



PHOTO NO. 15 - Close-up view of Photo No. 14.

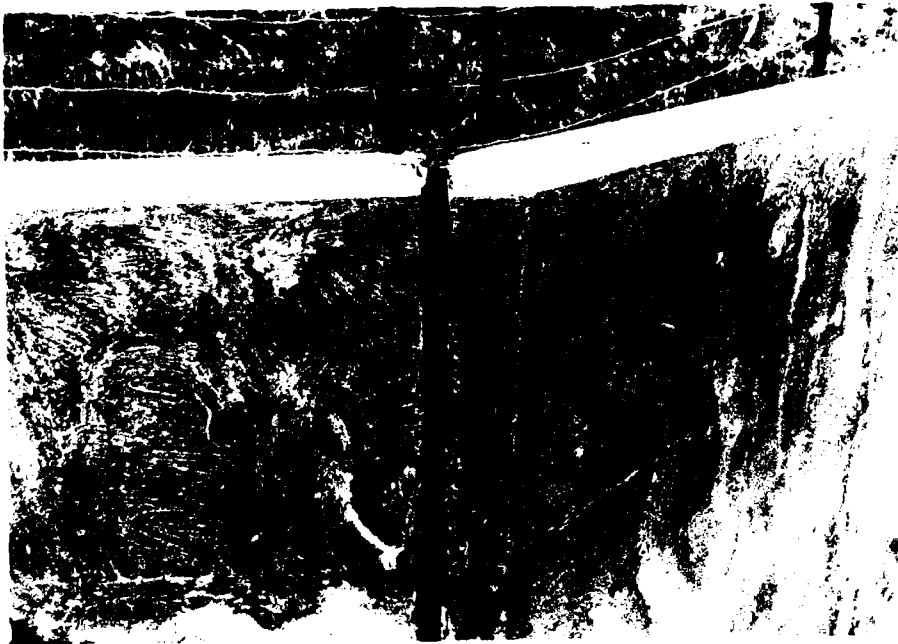


PHOTO NO. 16 - View of separation between left training wall and wingwall of outlet works.

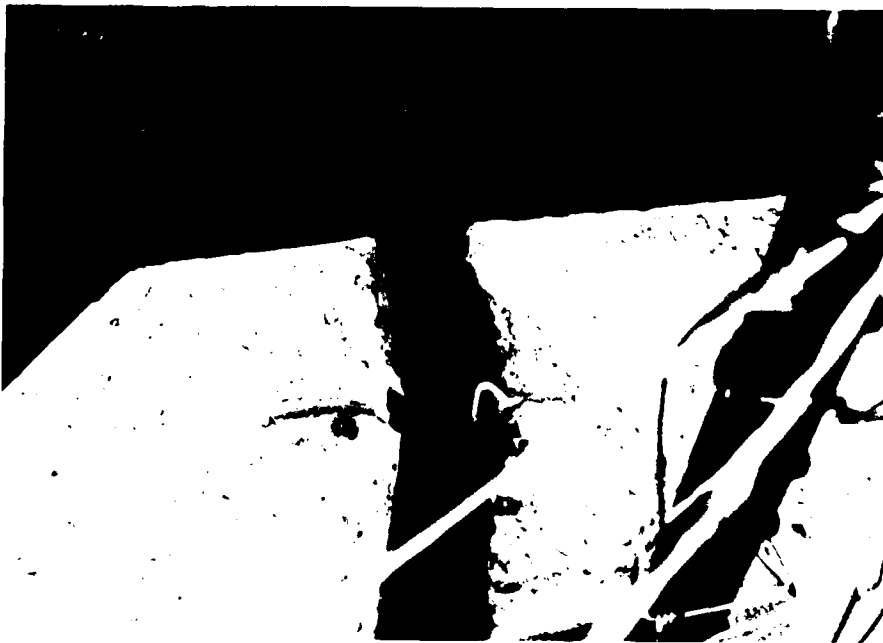


PHOTO NO. 17 - Close-up view of Photo No. 16.

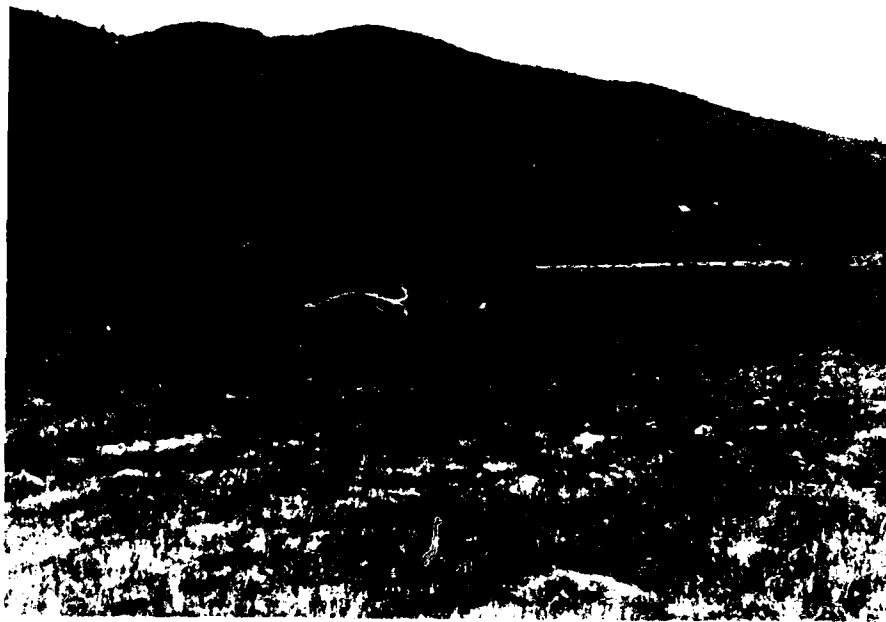


PHOTO NO. 18 - Entrance of emergency spillway from mid-channel of emergency spillway.



PHOTO NO. 19 - View of crest of emergency spillway from left abutment.



PHOTO NO. 20 - View of discharge area of emergency spillway  
from left downstream slope of dam.

APPENDIX D  
HYDROLOGIC AND HYDRAULIC COMPUTATIONS



<b>HNTB</b> HOWARD NEEDLES TAMMEN & BERGENDOFF For	Made by	RY	Date	6/1/79	Job No	5965-11-21
	Checked by	VIII	Date	6/1/79	Sheet No	1
Baker Dam Site # 8						

## HYDRAULICS & HYDROLOGY

Baker River Dam Site #8 Located on South Branch Baker River  
in the Town of Dorchester, N.H. in the  
Merrimack River Basin.

Classification: Size: intermediate  
Hazard: High

Basic Data: DA. 16.04 sq mi  
upstream catch slope 250 ft/mi  
Max elev - 2564 ft

Reservoir: Recreation Pool @ 1025 ft  
Storage 143 acre ft  
Emergency Spillway @ 1064.5 ft  
Storage 3760 acre ft  
Top of Dam @ 1070.5 ft  
Storage 4764 acre ft

Dam: Earth  
Length 1462 ft.  
Height 62 ft.

Spillways:  
Riser: Crest 1050.0 ft  
Length of weir: 30 ft  
Emergency: Crest 1064.5 ft  
width 400 ft

See Appendix "B" for plan of dam

<b>HNTB</b> HOWARD NEEDLES TAMMEN & BERGENDOFF	Made by	RY.	Date	6/1/79	JOB No	5965-11-01
	Checked by	V. D.	Date	6/4/79	Sheet No	2
For Baker 8						

## Step 1 Calculation of Test Flood Inflow

Classification : Size : Intermediate  
Hazard : High

Hydrologic Evaluation Guideline Recommends

PMF for Test Flood Inflow

The mountainous curve an average stream slope is 200 feet per mile.

$$\text{Test Flood} = 1810 \text{ csm} \times 16.04 \text{ sq mi} = 29,000 \text{ cfs}$$

at 19 inch runoff

As this is a flood control reservoir the portion of storage above the recreational pool can be used to store a portion of the PMF.

143 acre-ft at normal recreation pool level  
3760 acre-ft at crest of emergency spillway

3617 acre-ft available to store PMF

$$\begin{aligned} \text{Volume of PMF} &= \frac{19}{12} \text{ in/ft} \times 640 \frac{\text{acre}}{\text{mi}^2} \times 16.04 \text{ sq mi} \\ &= 16,254 \text{ acre-ft} \end{aligned}$$

<b>HNTB</b> HOWARD NEEDLES TAMMEN & BERGENDOFF For <u>Baker # 8</u>	Made by <u>RY</u>	Date <u>6/2/79</u>	Job No. <u>5765-11-01</u>
	Checked by <u>WVH</u>	Date <u>6/4/79</u>	Sheet No. <u>3</u>

## Step 2 Calculation of Test Flood Surchage

### Stage - Discharge Curve

<u>Elev.</u>	<u>Stage above Emer spillway</u>	<u>A. Riser Pipe Flow</u>	<u>B. Emergency Spillway</u>	<u>C. Crest of Dam</u>	<u>Total</u>
1064.5	0 ft	628 cfs	0	-	628 cfs
1066.	1.5	637	1530 cfs	-	2167
1068	3.5	648	6700	-	7348
1070	5.5	659	14,400	-	15,059
1072.5	6.0	661	16,650	-	17,311
1071.5	7.0	666	21,000	4518 cfs	26,184

A. From Baker River #8 Design Book, SES Durham, N.H.

See Calcs. in appendix

B Same as A

C. Computed as flow over broadcrested weir

$$Q = CLH^{3/2}$$

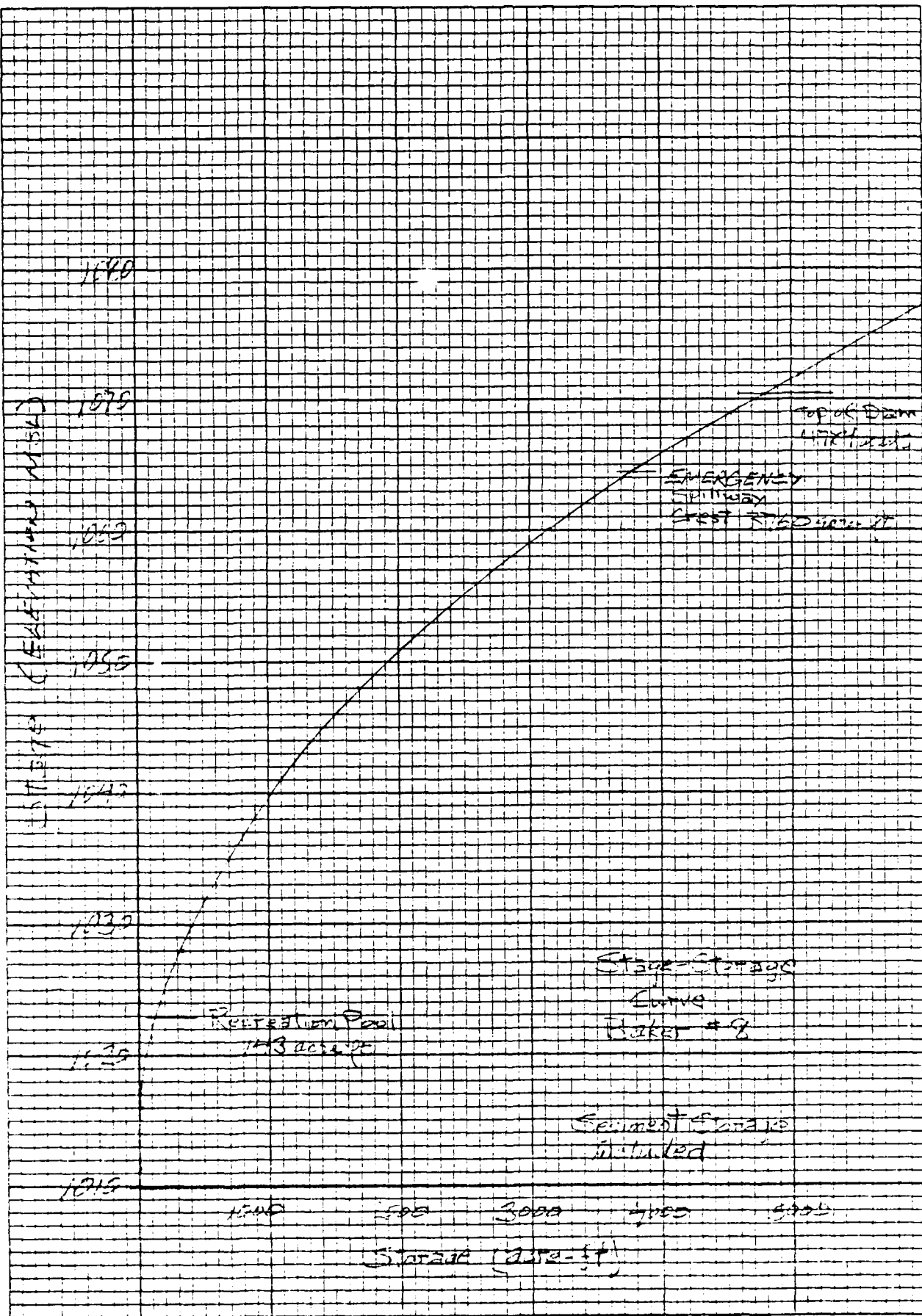
$$C = 3.09$$

$$L = 1462$$

$$Q = 4518 H^{3/2}$$

See figure 2 for Plot





1015

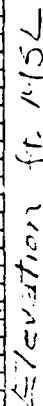


FIGURE 2

<b>HNTB</b> HOWARD NEEDLES TAMMEN & BERGENOFF For <u>Baker #8</u>	Made by <u>RY</u>	Date <u>5/31/79</u>	Job No <u>5965-11-01</u>
	Checked by <u>VW</u>	Date <u>6/4/79</u>	Sheet No <u>5</u>

## Estimate of Downstream Damage

### Step 1 Reservoir Storage

Top of Dam @ Elev. 1070.5  
Storage 4784 acre-ft

### Step 2 Breach Outflow

$$Q_{\text{Breach}} = 8/27 \sqrt{g} Y_0^{3/2} W_0$$

$W_0 = 40\%$  of length of dam

$Y_0 = \text{height} - \text{stream bed to max. pool elev. } 59 \text{ ft}$

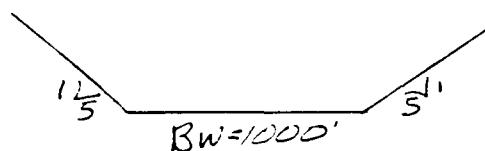
$$Q_{\text{Breach}} = 8/27 \sqrt{g} (40)(1462)(59)^{3/2} = 445,200 \text{ cfs}$$

Spillway discharge

$$Q_{p.} = \frac{16,600}{461,800 \text{ cfs}}$$

### Step 3 Stage-Discharge

Valley Section



Reach 1 = 8500 cfs

Schannel = .00475

$n = .05$

### Stage-Discharge

10 ft	104,100 cfs
15	195,600 cfs
20	311,700
25	456,500

<b>HNTB</b> HOWARD NEEDLES TAMMEN & BERGENDOFF For <u>Baker # 8</u>	Made by <u>RY</u>	Date <u>5/3/79</u>	Job No <u>5955-11-01</u>
	Checked by <u>VJH</u>	Date <u>6/1/79</u>	Sheet No <u>6</u>

Step 4 Reach Outflow  $S = 4784 \text{ acre ft}$   
 $Q_{P_1} = 461,800 \text{ cfs}$

Reach 1A  
 3550' of  
 2500' ft.

Stage = 25.1 ft area = 28,250 ft<sup>2</sup>  
 $V_1 = \frac{3550' \times 28250}{43560} = 2302 \text{ acre ft} < \frac{4784}{2}$

$Q_{P_2} = 461,800 \left(1 - \frac{2302}{4784}\right) = 239,600 \text{ cfs}$

Stage = 17.1 ft area = 18,562 ft<sup>2</sup>

$V_2 = \frac{3550 \times 18,562}{43560} = 1513 \text{ acre ft}$

$V_{ave} = 1907 \text{ acre ft}$

$Q_{P_2} = 461,800 \left(1 - \frac{1907}{4784}\right) = 277,700 \text{ cfs}$

Reach 1B  
 lower 24750' of  
 8500'

Stage = 18.7 ft area = 20,448 ft<sup>2</sup>

$V_2 = \frac{4950 \text{ ft} \times 20448}{43560} = 2323 \text{ acre ft} < \frac{4784}{2}$

$Q_{P_2} = 277,700 \text{ cfs} \left(1 - \frac{2323}{4784}\right) = 142,800 \text{ cfs}$

Stage = 12.7 ft area = 13,506 ft<sup>2</sup>

$V_2 = \frac{4950 \times 13506}{43560} = 1535 \text{ acre ft}$

$V_{ave} = 1929 \text{ acre ft}$

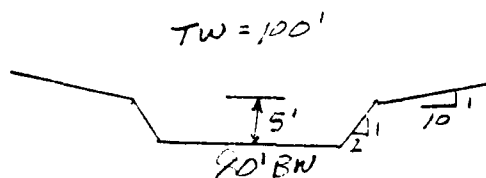
$Q_{P_2} = 277,700 \left(1 - \frac{1929}{4784}\right) = 155,700 \text{ cfs}$

Stage = 13.8 ft



<b>HNTB</b> HOWARD NEEDLES TAMMEN & BERGENDOFF	Made by <i>RY</i>	Date <i>5/31/79</i>	Job No <i>5365-11-01</i>
	Checked by <i>WLB</i>	Date <i>6/1/79</i>	Sheet No <i>7</i>
For <i>Raker # 8</i>			

Step 3 Reach 2 Length 1,500 feet



$$S_{channel} = 0.028\%$$

$$n_{ch} = .03$$

$$n_{ovb} = .08$$

### Stage - Discharge

10 ft	36,600 cfs
15	80,300
18	116,000
20	144,000
22	175,000

### Step 4

$$Q_{P1} = 165,700 \text{ cfs}$$

$$\text{Stage}_1 = 21.3 \text{ ft} \quad \text{area}_1 = 4740 \text{ ft}^2$$

$$V_1 = \frac{11,500 \times 4740}{43560} = 1251 \text{ sec/ft} < \frac{4740}{2}$$

$$Q_{P2T} = 165,700 \text{ cfs} \left(1 - \frac{1251}{4784}\right) = 122,370 \text{ cfs}$$

$$\text{Stage}_2 = 18.5 \text{ ft} \quad \text{area}_2 = 3620 \text{ ft}^2$$

$$V_2 = \frac{11,500 \times 3620}{43560} = 956 \text{ sec/ft}$$

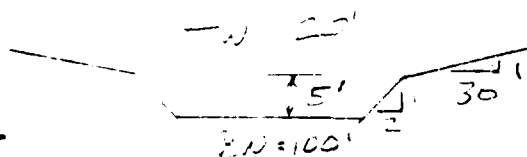
$$V_{ave} = 1103 \text{ sec/ft}$$

$$Q_{P2} = 165,700 \text{ cfs} \left(1 - \frac{1103}{4784}\right) = 127,500 \text{ cfs}$$

$$\text{Stage} = 18.8 \text{ ft.}$$

HNTB HOWARD NEEDLES TAMMEN & BERGENCOFF	Made by	RY	Date	5/31/79	Job No	535.5-11-21
	Checked by	VLP	Date	6/1/79	Sheet No	8

Step 3 Reach 3 Length 9000 ft



$$S_{channel} = .009\%$$

$$\eta_{ch} = .03$$

$$\eta_{os} = .08$$

Stage Discharge

10 ft	27,400 cfs
15	69,300
18	108,200
20	140,600

Step 4  $Q_{P_1} = 127,500$  cfs

$$Stage_1 = 19.2 \text{ ft}$$

$$area_1 = 8303 \text{ ft}^2$$

$$V_1 = \frac{9000 \times 8303}{43560} = 1715 \text{ sec-ft} \leftarrow \frac{4724}{2}$$

$$Q_{P_{2T}} = 127,500 \text{ cfs} \left( 1 - \frac{1715}{4724} \right) = 81,300 \text{ cfs}$$

$$Stage_2 = 16.1 \text{ ft}$$

$$area_2 = 5578 \text{ ft}^2$$

$$V_2 = \frac{9000 \times 5578}{43560} = 1152 \text{ sec-ft}$$

$$V_{ave} = 1434 \text{ sec-ft}$$

$$Q_{P_2} = 127,500 \left( 1 - \frac{1434}{4724} \right) = 89,300 \text{ cfs}$$

Stage 16.7 ft.

Summary

At dam

25.1 ft

1.5 mi d.s.

21.3 ft

3.7 mi d.s.

18.8 ft

At J 7 cfs

118 cfs

118 cfs

[illegible]

<b>HNTB</b> HOWARD NEEDLES TAMMEN & BERGENDOFF For <u>Baker #1</u>	Made by <u>FL</u>	Date <u>5/5/79</u>	Job No. <u>5955-2-1</u>
	Checked by <u>1/11</u>	Date <u>5/17/79</u>	Sheet No. <u>9</u>

1/2 PMF Surge Storage Effect

$$PMF = 29000 \text{ cfs} \quad 1/2 PMF = 14,500 \text{ cfs}$$

$$\text{Volume of } 1/2 PMF = 8127 \text{ acre-ft}$$

$$\text{Available Storage} = \text{Figure 2} - 143 \text{ acre-ft}$$

See pg. 4 for calculation of Stor(in)

$$R.O. = 9.5 \text{ inches}$$

$$Q_{P_2} = Q_{P_1} \times \left(1 - \frac{\text{Stor}}{9.5}\right)$$

<u>Elev</u>	<u>Stor(in)</u>	<u>Q<sub>P<sub>2</sub></sub></u>
1067	4.75	7250 cfs
1069	5.14	6650
1070	5.36	6320
1071.5	5.68	5830

See Figure 2 for Plot and final 1/2 PMF Outflow

$$\text{From Figure 2} \quad \text{Outflow} = 7,000 \text{ cfs}$$

$$\text{Stage} = 1067.9 \text{ ft}$$

2.6 ft below top of dam

5

1

1

1

1

6

1555

611

17

332

024

713

7161

1328

1115

012

7852

1112

子之

100

1



COMPUTATION SHEET  
SCS-522 REV 5-58

U. S. DEPARTMENT OF AGRICULTURE  
SOIL CONSERVATION SERVICE

STATE ALA PROJECT 5 - 5112-1-1  
BY W. H. H. DATE 1-10-65 CHECKED BY W. H. H. DATE 1-10-65  
SUBJECT WATERWAY REPAIRS SHEET 1 OF 1

FLOW CONSTANT

$$Q = C A \sqrt{2gh}$$

$$A = \frac{Q}{C \sqrt{2gh}}$$

$$Q = 237 \text{ CFS}$$

$$C = 0.67$$

$$h = 1050.0 - 1022.0 = 28.0 \text{ FT}$$

$$\text{ASSUME } 26.3 \text{ FT TO } Q$$

$$\text{OF CENTER}$$

$$A = \frac{237}{0.67 \sqrt{2(32.2)(26.3)}} = \frac{237}{57.60} = 4.11 \text{ FT}^2$$

$$WCE = 2 - 3.02 \times 1.42 = 1.57 \text{ FEET}$$

$$H = 2 - 3.02 \times 1.42 = 1.57 \text{ FEET OK}$$

FOR INTERMEDIATE POINTS

$$Q = (C)(A)(\sqrt{2gh})$$

$$Q = 4.11 \text{ FT}^2$$

WCE HWO HWL Q

1043.0

1043.7

1044.4

1045.1

1045.8

1046.5

1047.2

1047.9

1048.6

1049.3

0

0.7

1

2

3

4

5

6

7

0

0.93

1.87

2.80

3.74

4.67

5.61

6.54

7.48

0

35.2

40.3

45.4

50.5

55.6

60.7

65.8

70.9

237



7-17-65  
1/24/65  
1-17-65

SITE 5 N. 4. 654

NUMBER RUNS 1116000000 SHEET 11

AVERAGE RUN RATE 0.910 CC 0.10 % CORRECTION

STAGE	STAGE	Q <sub>s</sub>	Q <sub>s</sub>	AVG	TIME
1050	1050	215	200.5	203	11.16
1052	1052	247	240.5	219	10.25
1042	1042	215	200.5	203	10.25
1040	1040	215	200.5	203	10.25
1036	1036	204	200.5	199	10.10
1032	1032	171	200.5	177	10.75
1028	1028	141	200.5	147	10.61
1024.4	1024.4				10.56

(1010-171) 12.16 = 1027(10.00) 10.25 10.25 10.25

AVERAGE RATE 1027.12 = 1027.12 10.25

AVERAGE RATE 1027.12 = 1027.12 10.25

USING 1027.12 AS AVERAGE

1027.12 10.25 = 1027.12 10.25

1027.12 10.25 = 1027.12 10.25

1027.12 10.25 = 1027.12 10.25

U S DEPARTMENT OF AGRICULTURE  
SOIL CONSERVATION SERVICE

تاریخ: ۱۵/۱۲/۱۴۰۲

$$VOL\ OF\ SURF\ MEDIUM = 199 \times 0.72 = 143.3 \text{ LBS} \quad 145 \text{ GALL}$$

POB OF INDIANAS CO. =  $199 \times 0.25 = 50.7$  WGS. 56 ACFT

FROM STAGE STORAGE CURVE

123 NO. 17 OF 1902 - AT MUMBAI 10/2/02

مجلس علماء وادباء

2.0455 - 2.0465 = FROM NOZZLE PLATE

১০৬ পৃষ্ঠা

2047-25-10-1710.9 AC-FR

455 111 42 27

TOTAL STORAGE AREA TO WHICH ATTEND

SECRET

020705Z JUL 68 0000Z 0000Z 0000Z 0000Z 0000Z 0000Z

Stewart, William A. . . . .

TOTAL 1910 10-87

[illegible]

1994-1995

CONFIDENTIAL SOURCE OF INFO. 1050.0

TYPE SPECIES: L. 200423 - 1910 - 1001

COMPUTATION SHEET  
SCS-522 REV 5-58

U. S. DEPARTMENT OF AGRICULTURE  
SOIL CONSERVATION SERVICE

STATE N. H. PROJECT CLARK RIVER WATERWAY  
BY W. J. H. J. DATE 11-3-64 CHECKED BY T. J. H. DATE 1/65 JOB NO. 44-1-52  
SUBJECT LOW STAGE ORIFICE - SIZE SHEET 14 OF 14

TOTAL RELEASE RATE = 237 CFS - FROM WOLF-PAN

INVERT ELEV - HIGH STAGE = 1050.0

" " - LOW STAGE = 1023.0

DIFF. IN ELEV = 27.0 FT

FOR ORIFICE FLOW  $Q = C A \sqrt{2gh}$

$Q = 237 \text{ CFS}$

$C = 0.67 \text{ CFS}$

$\sqrt{2g} = 8.02$

$h = 27.0 - 0.5 \text{ (DEPTH OF LOW STAGE ORIFICE)}$

TRY 2 - 3.02' X 1.42' OPENINGS

$A = 8.58$

$h = 27.00 - 0.71 = 26.29$

$Q = 0.67 \times 8.58 \times 8.02 \times (26.29)^{1/2} = 513$

$C_u = 4610 (A^2 \cdot 513) = 234.59$

USE 2 - 3.02' X 1.42' } OPENINGS  
3'-0 1/2" X 1'-5"

OR  
1 - 6.04' X 1.42' } OPENING  
6'-0 1/2" X 1'-5"

WATER FLOW

$Q = 237$

$C = 31$

$A = 2.4302 \text{ (sq ft)}$

$Q = 15.72 \text{ (sq ft)}$

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SMITH 60

32. 232

$$G = \mathbb{Z}/4\mathbb{Z}$$

$$C_p = \sqrt{\frac{2 \cdot \rho \cdot V^2}{\rho \cdot C_p \cdot A \cdot (V - V_{\infty})^2}}$$

$$C_p = \sqrt{\frac{1.0 + (0.025)(4.2)}{1.0 + (0.025)(4.2) + \frac{1.0}{(0.025)(4.2)}}}$$

$$C_p = \sqrt{\frac{24.120.17}{12.500.000 + 2.500.000}}$$

$$C_p = \sqrt{\frac{240000}{3.466}}$$

$$C_p = \sqrt{7,167.05}$$

$C_p = 14.66$

5057

2000

As follows:

1. *Journal of the American Medical Association*, 1997; 277: 1025-1030.

1990

*Journal of Management Education*

1. 2. 3.

17. 100 100 100

Q. 150 (2012-3)

1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30. 31. 32. 33. 34. 35. 36. 37. 38. 39. 40. 41. 42. 43. 44. 45. 46. 47. 48. 49. 50. 51. 52. 53. 54. 55. 56. 57. 58. 59. 60. 61. 62. 63. 64. 65. 66. 67. 68. 69. 70. 71. 72. 73. 74. 75. 76. 77. 78. 79. 80. 81. 82. 83. 84. 85. 86. 87. 88. 89. 90. 91. 92. 93. 94. 95. 96. 97. 98. 99. 100.

$$F_2 = \frac{160}{20} = \frac{75.23}{20} = 1.875$$

$$r_2 = \frac{216 \pm \sqrt{3.072}}{(1.375)^{1/2}}$$

$$K_c = \frac{0.0125}{0.512}$$

$\rho_c = 0.0119$

1. 1500

$$G = 14.66 \left[ \frac{100000 - (100000 - 100000)}{100000} \right]^{1/2} = 14.66 (100000)^{1/2}$$

$$C_1 = 94.66 \times 7.42 = 6.97 \text{ CAS} + 715 \text{ CAS}$$

66" RCP PROVIDES 7500 CFS WHICH IS 7 TIMES  
SO USE 60" RCP AND PUMPED ADDITIONAL  
STORAGE TO BE CONSIDERED

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| Station | Time  | Lat       | Long       | Alt | Wind | Temp | Humid | Clouds | Remarks |
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| 1       | 0800  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 2       | 0900  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 3       | 1000  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 4       | 1100  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 5       | 1200  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 6       | 1300  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 7       | 1400  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 8       | 1500  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 9       | 1600  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 10      | 1700  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 11      | 1800  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 12      | 1900  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 13      | 2000  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 14      | 2100  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 15      | 2200  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 16      | 2300  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 17      | 2400  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 18      | 2500  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 19      | 2600  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 20      | 2700  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 21      | 2800  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 22      | 2900  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 23      | 3000  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 24      | 3100  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 25      | 3200  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 26      | 3300  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 27      | 3400  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 28      | 3500  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 29      | 3600  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 30      | 3700  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 31      | 3800  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 32      | 3900  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 33      | 4000  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 34      | 4100  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 35      | 4200  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 36      | 4300  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 37      | 4400  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 38      | 4500  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 39      | 4600  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 40      | 4700  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 41      | 4800  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 42      | 4900  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 43      | 5000  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 44      | 5100  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 45      | 5200  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 46      | 5300  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 47      | 5400  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 48      | 5500  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 49      | 5600  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 50      | 5700  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 51      | 5800  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 52      | 5900  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 53      | 6000  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 54      | 6100  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 55      | 6200  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 56      | 6300  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 57      | 6400  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 58      | 6500  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 59      | 6600  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 60      | 6700  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 61      | 6800  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 62      | 6900  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 63      | 7000  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 64      | 7100  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 65      | 7200  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 66      | 7300  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 67      | 7400  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 68      | 7500  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 69      | 7600  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 70      | 7700  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 71      | 7800  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 72      | 7900  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 73      | 8000  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 74      | 8100  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 75      | 8200  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 76      | 8300  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 77      | 8400  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 78      | 8500  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 79      | 8600  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 80      | 8700  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 81      | 8800  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 82      | 8900  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 83      | 9000  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 84      | 9100  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 85      | 9200  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 86      | 9300  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 87      | 9400  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 88      | 9500  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 89      | 9600  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 90      | 9700  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 91      | 9800  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 92      | 9900  | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 93      | 10000 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 94      | 10100 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 95      | 10200 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 96      | 10300 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 97      | 10400 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 98      | 10500 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 99      | 10600 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 100     | 10700 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 101     | 10800 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 102     | 10900 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 103     | 11000 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 104     | 11100 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 105     | 11200 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 106     | 11300 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 107     | 11400 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 108     | 11500 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 109     | 11600 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 110     | 11700 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 111     | 11800 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 112     | 11900 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 113     | 12000 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 114     | 12100 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 115     | 12200 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 116     | 12300 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 117     | 12400 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 118     | 12500 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 119     | 12600 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 120     | 12700 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 121     | 12800 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 122     | 12900 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 123     | 13000 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 124     | 13100 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 125     | 13200 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 126     | 13300 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 127     | 13400 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 128     | 13500 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 129     | 13600 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 130     | 13700 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 131     | 13800 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 132     | 13900 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 133     | 14000 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 134     | 14100 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 135     | 14200 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 136     | 14300 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 137     | 14400 | 34° 15' N | 122° 00' W | 10  | 10   | 55   | 85    | 100    | Clear   |
| 138     | 14500 | 34° 15' N | 122° 00' W |     |      |      |       |        |         |



JOEL COMMUNICATIONS SERVICE

| DATE | 1/5 | 2/1 | 3/1 | 4/1 | 5/1 | 6/1 | 7/1 | 8/1 | 9/1 | 10/1 | 11/1 | 12/1 | 1/2 | 2/2 | 3/2 | 4/2 | 5/2 | 6/2 | 7/2 | 8/2 | 9/2 | 10/2 | 11/2 | 12/2 | 1/3 | 2/3 | 3/3 | 4/3 | 5/3 | 6/3 | 7/3 | 8/3 | 9/3 | 10/3 | 11/3 | 12/3 | 1/4 | 2/4 | 3/4 | 4/4 | 5/4 | 6/4 | 7/4 | 8/4 | 9/4 | 10/4 | 11/4 | 12/4 | 1/5 | 2/5 | 3/5 | 4/5 | 5/5 | 6/5 | 7/5 | 8/5 | 9/5 | 10/5 | 11/5 | 12/5 | 1/6 | 2/6 | 3/6 | 4/6 | 5/6 | 6/6 | 7/6 | 8/6 | 9/6 | 10/6 | 11/6 | 12/6 | 1/7 | 2/7 | 3/7 | 4/7 | 5/7 | 6/7 | 7/7 | 8/7 | 9/7 | 10/7 | 11/7 | 12/7 | 1/8 | 2/8 | 3/8 | 4/8 | 5/8 | 6/8 | 7/8 | 8/8 | 9/8 | 10/8 | 11/8 | 12/8 | 1/9 | 2/9 | 3/9 | 4/9 | 5/9 | 6/9 | 7/9 | 8/9 | 9/9 | 10/9 | 11/9 | 12/9 | 1/10 | 2/10 | 3/10 | 4/10 | 5/10 | 6/10 | 7/10 | 8/10 | 9/10 | 10/10 | 11/10 | 12/10 | 1/11 | 2/11 | 3/11 | 4/11 | 5/11 | 6/11 | 7/11 | 8/11 | 9/11 | 10/11 | 11/11 | 12/11 | 1/12 | 2/12 | 3/12 | 4/12 | 5/12 | 6/12 | 7/12 | 8/12 | 9/12 | 10/12 | 11/12 | 12/12 | 1/13 | 2/13 | 3/13 | 4/13 | 5/13 | 6/13 | 7/13 | 8/13 | 9/13 | 10/13 | 11/13 | 12/13 | 1/14 | 2/14 | 3/14 | 4/14 | 5/14 | 6/14 | 7/14 | 8/14 | 9/14 | 10/14 | 11/14 | 12/14 | 1/15 | 2/15 | 3/15 | 4/15 | 5/15 | 6/15 | 7/15 | 8/15 | 9/15 | 10/15 | 11/15 | 12/15 | 1/16 | 2/16 | 3/16 | 4/16 | 5/16 | 6/16 | 7/16 | 8/16 | 9/16 | 10/16 | 11/16 | 12/16 | 1/17 | 2/17 | 3/17 | 4/17 | 5/17 | 6/17 | 7/17 | 8/17 | 9/17 | 10/17 | 11/17 | 12/17 | 1/18 | 2/18 | 3/18 | 4/18 | 5/18 | 6/18 | 7/18 | 8/18 | 9/18 | 10/18 | 11/18 | 12/18 | 1/19 | 2/19 | 3/19 | 4/19 | 5/19 | 6/19 | 7/19 | 8/19 | 9/19 | 10/19 | 11/19 | 12/19 | 1/20 | 2/20 | 3/20 | 4/20 | 5/20 | 6/20 | 7/20 | 8/20 | 9/20 | 10/20 | 11/20 | 12/20 | 1/21 | 2/21 | 3/21 | 4/21 | 5/21 | 6/21 | 7/21 | 8/21 | 9/21 | 10/21 | 11/21 | 12/21 | 1/22 | 2/22 | 3/22 | 4/22 | 5/22 | 6/22 | 7/22 | 8/22 | 9/22 | 10/22 | 11/22 | 12/22 | 1/23 | 2/23 | 3/23 | 4/23 | 5/23 | 6/23 | 7/23 | 8/23 | 9/23 | 10/23 | 11/23 | 12/23 | 1/24 | 2/24 | 3/24 | 4/24 | 5/24 | 6/24 | 7/24 | 8/24 | 9/24 | 10/24 | 11/24 | 12/24 | 1/25 | 2/25 | 3/25 | 4/25 | 5/25 | 6/25 | 7/25 | 8/25 | 9/25 | 10/25 | 11/25 | 12/25 | 1/26 | 2/26 | 3/26 | 4/26 | 5/26 | 6/26 | 7/26 | 8/26 | 9/26 | 10/26 | 11/26 | 12/26 | 1/27 | 2/27 | 3/27 | 4/27 | 5/27 | 6/27 | 7/27 | 8/27 | 9/27 | 10/27 | 11/27 | 12/27 | 1/28 | 2/28 | 3/28 | 4/28 | 5/28 | 6/28 | 7/28 | 8/28 | 9/28 | 10/28 | 11/28 | 12/28 | 1/29 | 2/29 | 3/29 | 4/29 | 5/29 | 6/29 | 7/29 | 8/29 | 9/29 | 10/29 | 11/29 | 12/29 | 1/30 | 2/30 | 3/30 | 4/30 | 5/30 | 6/30 | 7/30 | 8/30 | 9/30 | 10/30 | 11/30 | 12/30 | 1/31 | 2/31 | 3/31 | 4/31 | 5/31 | 6/31 | 7/31 | 8/31 | 9/31 | 10/31 | 11/31 | 12/31 | 1/32 | 2/32 | 3/32 | 4/32 | 5/32 | 6/32 | 7/32 | 8/32 | 9/32 | 10/32 | 11/32 | 12/32 | 1/33 | 2/33 | 3/33 | 4/33 | 5/33 | 6/33 | 7/33 | 8/33 | 9/33 | 10/33 | 11/33 | 12/33 | 1/34 | 2/34 | 3/34 | 4/34 | 5/34 | 6/34 | 7/34 | 8/34 | 9/34 | 10/34 | 11/34 | 12/34 | 1/35 | 2/35 | 3/35 | 4/35 | 5/35 | 6/35 | 7/35 | 8/35 | 9/35 | 10/35 | 11/35 | 12/35 | 1/36 | 2/36 | 3/36 | 4/36 | 5/36 | 6/36 | 7/36 | 8/36 | 9/36 | 10/36 | 11/36 | 12/36 | 1/37 | 2/37 | 3/37 | 4/37 | 5/37 | 6/37 | 7/37 | 8/37 | 9/37 | 10/37 | 11/37 | 12/37 | 1/38 | 2/38 | 3/38 | 4/38 | 5/38 | 6/38 | 7/38 | 8/38 | 9/38 | 10/38 | 11/38 | 12/38 | 1/39 | 2/39 | 3/39 | 4/39 | 5/39 | 6/39 | 7/39 | 8/39 | 9/39 | 10/39 | 11/39 | 12/39 | 1/40 | 2/40 | 3/40 | 4/40 | 5/40 | 6/40 | 7/40 | 8/40 | 9/40 | 10/40 | 11/40 | 12/40 | 1/41 | 2/41 | 3/41 | 4/41 | 5/41 | 6/41 | 7/41 | 8/41 | 9/41 | 10/41 | 11/41 | 12/41 | 1/42 | 2/42 | 3/42 | 4/42 | 5/42 | 6/42 | 7/42 | 8/42 | 9/42 | 10/42 | 11/42 | 12/42 | 1/43 | 2/43 | 3/43 | 4/43 | 5/43 | 6/43 | 7/43 | 8/43 | 9/43 | 10/43 | 11/43 | 12/43 | 1/44 | 2/44 | 3/44 | 4/44 | 5/44 | 6/44 | 7/44 | 8/44 | 9/44 | 10/44 | 11/44 | 12/44 | 1/45 | 2/45 | 3/45 | 4/45 | 5/45 | 6/45 | 7/45 | 8/45 | 9/45 | 10/45 | 11/45 | 12/45 | 1/46 | 2/46 | 3/46 | 4/46 | 5/46 | 6/46 | 7/46 | 8/46 | 9/46 | 10/46 | 11/46 | 12/46 | 1/47 | 2/47 | 3/47 | 4/47 | 5/47 | 6/47 | 7/47 | 8/47 | 9/47 | 10/47 | 11/47 | 12/47 | 1/48 | 2/48 | 3/48 | 4/48 | 5/48 | 6/48 | 7/48 | 8/48 | 9/48 | 10/48 | 11/48 | 12/48 | 1/49 | 2/49 | 3/49 | 4/49 | 5/49 | 6/49 | 7/49 | 8/49 | 9/49 | 10/49 | 11/49 | 12/49 | 1/50 | 2/50 | 3/50 | 4/50 | 5/50 | 6/50 | 7/50 | 8/50 | 9/50 | 10/50 | 11/50 | 12/50 | 1/51 | 2/51 | 3/51 | 4/51 | 5/51 | 6/51 | 7/51 | 8/51 | 9/51 | 10/51 | 11/51 | 12/51 | 1/52 | 2/52 | 3/52 | 4/52 | 5/52 | 6/52 | 7/52 | 8/52 | 9/52 | 10/52 | 11/52 | 12/52 | 1/53 | 2/53 | 3/53 | 4/53 | 5/53 | 6/53 | 7/53 | 8/53 | 9/53 | 10/53 | 11/53 | 12/53 | 1/54 | 2/54 | 3/54 | 4/54 | 5/54 | 6/54 | 7/54 | 8/54 | 9/54 | 10/54 | 11/54 | 12/54 | 1/55 | 2/55 | 3/55 | 4/55 | 5/55 | 6/55 | 7/55 | 8/55 | 9/55 | 10/55 | 11/55 | 12/55 | 1/56 | 2/56 | 3/56 | 4/56 | 5/56 | 6/56 | 7/56 | 8/56 | 9/56 | 10/56 | 11/56 | 12/56 | 1/57 | 2/57 | 3/57 | 4/57 | 5/57 | 6/57 | 7/57 | 8/57 | 9/57 | 10/57 | 11/57 | 12/57 | 1/58 | 2/58 | 3/58 | 4/58 | 5/58 | 6/58 | 7/58 | 8/58 | 9/58 | 10/58 | 11/58 | 12/58 | 1/59 | 2/59 | 3/59 | 4/59 | 5/59 | 6/59 | 7/59 | 8/59 | 9/59 | 10/59 | 11/59 | 12/59 | 1/60 | 2/60 | 3/60 | 4/60 | 5/60 | 6/60 | 7/60 | 8/60 | 9/60 | 10/60 | 11/60 | 12/60 | 1/61 | 2/61 | 3/61 | 4/61 | 5/61 | 6/61 | 7/61 | 8/61 | 9/61 | 10/61 | 11/61 | 12/61 | 1/62 | 2/62 | 3/62 | 4/62 | 5/62 | 6/62 | 7/62 | 8/62 | 9/62 | 10/62 | 11/62 | 12/62 | 1/63 | 2/63 | 3/63 | 4/63 | 5/63 | 6/63 | 7/63 | 8/63 | 9/63 | 10/63 | 11/63 | 12/63 | 1/64 | 2/64 | 3/64 | 4/64 | 5/64 | 6/64 | 7/64 | 8/64 | 9/64 | 10/64 | 11/64 | 12/64 | 1/65 | 2/65 | 3/65 | 4/65 | 5/65 | 6/65 | 7/65 | 8/65 | 9/65 | 10/65 | 11/65 | 12/65 | 1/66 | 2/66 | 3/66 | 4/66 | 5/66 | 6/66 | 7/66 | 8/66 | 9/66 | 10/66 | 11/66 | 12/66 | 1/67 | 2/67 | 3/67 | 4/67 | 5/67 | 6/67 | 7/67 | 8/67 | 9/67 | 10/67 | 11/67 | 12/67 | 1/68 | 2/68 | 3/68 | 4/68 | 5/68 | 6/68 | 7/68 | 8/68 | 9/68 | 10/68 | 11/68 | 12/68 | 1/69 | 2/69 | 3/69 | 4/69 | 5/69 | 6/69 | 7/69 | 8/69 | 9/69 | 10/69 | 11/69 | 12/69 | 1/70 | 2/70 | 3/70 | 4/70 | 5/70 | 6/70 | 7/70 | 8/70 | 9/70 | 10/70 | 11/70 | 12/70 | 1/71 | 2/71 | 3/71 | 4/71 | 5/71 | 6/71 | 7/71 | 8/71 | 9/71 | 10/71 | 11/71 | 12/71 | 1/72 | 2/72 | 3/72 | 4/72 | 5/72 | 6/72 | 7/72 | 8/72 | 9/72 | 10/72 | 11/72 | 12/72 | 1/73 | 2/73 | 3/73 | 4/73 | 5/73 | 6/73 | 7/73 | 8/73 | 9/73 | 10/73 | 11/73 | 12/73 | 1/74 | 2/74 | 3/74 | 4/74 | 5/74 | 6/74 | 7/74 | 8/74 | 9/74 | 10/74 | 11/74 | 12/74 | 1/75 | 2/75 | 3/75 | 4/75 | 5/75 | 6/75 | 7/75 | 8/75 | 9/75 | 10/75 | 11/75 | 12/75 | 1/76 | 2/76 | 3/76 | 4/76 | 5/76 | 6/76 | 7/76 | 8/76 | 9/76 | 10/76 | 11/76 | 12/76 | 1/77 | 2/77 | 3/77 | 4/77 | 5/77 | 6/77 | 7/77 | 8/77 | 9/77 | 10/77 | 11/77 | 12/77 | 1/78 | 2/78 | 3/78 | 4/78 | 5/78 | 6/78 | 7/78 | 8/78 | 9/78 | 10/78 | 11/78 | 12/78 | 1/79 | 2/79 | 3/79 | 4/79 | 5/79 | 6/79 | 7/79 | 8/79 | 9/79 | 10/79 | 11/79 | 12/79 | 1/80 | 2/80 | 3/80 | 4/80 | 5/80 | 6/80 | 7/80 | 8/80 | 9/80 | 10/80 | 11/80 | 12/80 | 1/81 | 2/81 | 3/81 | 4/81 | 5/81 | 6/81 | 7/81 | 8/81 | 9/81 | 10/81 | 11/81 | 12/81 | 1/82 | 2/82 | 3/82 | 4/82 | 5/82 | 6/82 | 7/82 | 8/82 | 9/82 | 10/82 | 11/82 | 12/82 | 1/83 | 2/83 | 3/83 | 4/83 | 5/83 | 6/83 | 7/83 | 8/83 | 9/83 | 10/83 | 11/83 | 12/83 | 1/84 | 2/84 | 3/84 | 4/84 | 5/84 | 6/84 | 7/84 | 8/84 | 9/84 | 10/84 | 11/84 | 12/84 | 1/85 | 2/85 | 3/85 | 4/85 | 5/85 | 6/85 | 7/85 | 8/85 | 9/85 | 10/85 | 11/85 | 12/85 | 1/86 | 2/86 | 3/86 | 4/86 | 5/86 | 6/86 | 7/86 | 8/86 | 9/86 | 10/86 | 11/86 | 12/86 | 1/87 | 2/87 | 3/87 | 4/87 | 5/87 | 6/87 | 7/87 | 8/87 | 9/87 | 10/87 | 11/87 | 12/87 | 1/88 | 2/88 | 3/88 | 4/88 | 5/88 | 6/88 | 7/88 | 8/88 | 9/88 | 10/88 | 11/88 | 12/88 | 1/89 | 2/89 | 3/89 | 4/89 | 5/89 | 6/89 | 7/89 | 8/89 | 9/89 | 10/89 | 11/89 | 12/89 | 1/90 | 2/90 | 3/90 | 4/90 | 5/90 | 6/90 | 7/90 | 8/90 | 9/90 | 10/90 | 11/90 | 12/90 | 1/91 | 2/91 | 3/91 | 4/91 | 5/91 | 6/91 | 7/91 | 8/91 | 9/91 | 10/91 | 11/91 | 12/91 | 1/92 | 2/92 | 3/92 | 4/92 | 5/92 | 6/92 | 7/92 | 8/92 | 9/92 | 10/92 | 11/92 | 12/92 | 1/93 | 2/93 | 3/93 | 4/93 | 5/93 | 6/93 | 7/93 | 8/93 | 9/93 | 10/93 | 11/93 | 12/93 | 1/94 | 2/94 | 3/94 | 4/94 | 5/94 | 6/94 | 7/94 | 8/94 | 9/94 | 10/94 | 11/94 | 12/94 | 1/95 | 2/95 | 3/95 | 4/95 | 5/95 | 6/95 | 7/95 | 8/95 | 9/95 | 10/95 | 11/95 | 12/95 | 1/96 | 2/96 | 3/96 | 4/96 | 5/96 | 6/96 | 7/96 | 8/96 | 9/96 | 10/96 | 11/96 | 12/96 | 1/97 | 2/97 | 3/97 | 4/97 | 5/97 | 6/97 | 7/97 | 8/97 | 9/97 | 10/97 | 11/97 | 12/97 | 1/98 | 2/98 | 3/98 | 4/98 | 5/98 | 6/98 | 7/98 | 8/98 | 9/98 | 10/98 | 11/98 | 12/98 | 1/99 | 2/99 | 3/99 | 4/99 | 5/99 | 6/99 | 7/99 | 8/99 | 9/99 | 10/99 | 11/99 | 12/99 | 1/100 | 2/100 | 3/100 | 4/100 | 5/100 | 6/100 | 7/100 | 8/100 | 9/100 | 10/100 | 11/100 | 12/100 | 1/101 | 2/101 | 3/101 | 4/101 | 5/101 | 6/101 | 7/101 | 8/101 | 9/101 | 10/101 | 11/101 | 12/101 | 1/102 | 2/102 | 3/102 | 4/102 | 5/102 | 6/102 | 7/102 | 8/102 | 9/102 | 10/102 | 11/102 | 12/102 | 1/103 | 2/103 | 3/103 | 4/103 | 5/103 | 6/103 | 7/103 | 8/103 | 9/103 | 10/103 | 11/103 | 12/103 | 1/104 | 2/104 | 3/104 | 4/104 | 5/104 | 6/104 | 7/104 | 8/104 | 9/104 | 10/104 | 11/104 | 12/104 | 1/105 | 2/105 | 3/105 | 4/105 | 5/105 | 6/105 | 7/105 | 8/105 | 9/105 | 10/105 | 11/105 | 12/105 | 1/106 | 2/106 | 3/106 | 4/106 | 5/106 | 6/106 | 7/106 | 8/106 | 9/106 | 10/106 | 11/106 | 12/106 | 1/107 | 2/107 | 3/107 | 4/107 | 5/107 | 6/107 | 7/107 | 8/107 | 9/107 | 10/107 | 11/107 | 12/107 | 1/108 | 2/108 | 3/108 | 4/108 | 5/108 | 6/108 | 7/108 | 8/108 | 9/108 | 10/108 | 11/108 | 12/108 | 1/109 | 2/109 | 3/109 | 4/109 | 5/109 | 6/109 | 7/109 | 8/109 | 9/109 | 10/109 | 11/109 | 12/109 |
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AD-A156 414

NATIONAL PROGRAM FOR INSPECTION OF NON-FEDERAL DAMS  
BAKER FLOODWATER RESE. (U) CORPS OF ENGINEERS WALTHAM  
MA NEW ENGLAND DIV JUN 79

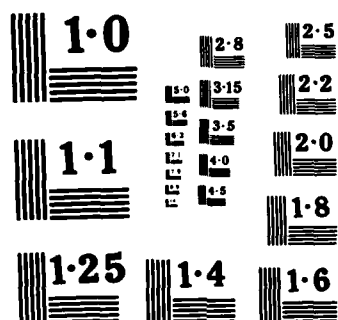
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UNCLASSIFIED

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NL





NATIONAL BUREAU OF STANDARDS  
MICROCOPY RESOLUTION TEST CHART

NO. 144 5-57  
Tactical Computations

U. S. DEPARTMENT OF AGRICULTURE  
SOIL CONSERVATION SERVICE

N. H. 654

10-13-65

11/15

TOPOGRAPHIC

100' WIDE ROAD 100' WIDE ROAD 100' WIDE ROAD

SHEET 31

| STATION | GRADE | AREA<br>SQUARE<br>Feet | 10"<br>RCP<br>G | TOTAL<br>G |  |  |  |  |
|---------|-------|------------------------|-----------------|------------|--|--|--|--|
|         |       | CFS                    | CFS             | CFS        |  |  |  |  |
| 101.0   | 55.0  | 2                      | 105.15          | 105.15     |  |  |  |  |
| 102.0   | 55.5  | 2                      | 130.75          | 130.75     |  |  |  |  |
| 103.0   | 56.0  | 2                      | 132.25          | 132.25     |  |  |  |  |
| 104.0   | 56.5  | 2                      | 134.40          | 134.40     |  |  |  |  |
| 105.0   | 57.0  | 2                      | 139.15          | 139.15     |  |  |  |  |
| 106.0   | 57.5  | 2                      | 141.75          | 141.75     |  |  |  |  |
| 107.0   | 58.0  | 2                      | 145.00          | 145.00     |  |  |  |  |
| 108.0   | 58.5  | 2                      | 147.45          | 147.45     |  |  |  |  |
| 109.0   | 59.0  | 2                      | 150.75          | 150.75     |  |  |  |  |
| 110.0   | 59.5  | 2                      | 152.75          | 152.75     |  |  |  |  |
| 111.0   | 60.0  | 2                      | 155.00          | 155.00     |  |  |  |  |
| 112.0   | 60.5  | 2                      | 157.45          | 157.45     |  |  |  |  |
| 113.0   | 61.0  | 2                      | 161.75          | 161.75     |  |  |  |  |
| 114.0   | 61.5  | 2                      | 163.75          | 163.75     |  |  |  |  |
| 115.0   | 62.0  | 2                      | 165.75          | 165.75     |  |  |  |  |

STAGE DISCHARGE CURVE

FOR FLOOD ROUTING

SHEET 33

2115 B

RAISED GRADE WATERWAYS

| STAGE  | Q       | STAGE  | Q      | STAGE  | Q      | STAGE  | Q         |
|--------|---------|--------|--------|--------|--------|--------|-----------|
| FEET   | CFS     | FEET   | CFS    | FEET   | CFS    | FEET   | CFS       |
| 1023.0 | 0       | 1023.5 | 227.07 | 1024.0 | 571.35 | 1024.5 | 1505.65   |
| 1023.2 | 1.45    | 1024.0 | 231.55 | 1024.5 | 550.77 | 1025.0 | 17221.19  |
| 1023.4 | 4.45    | 1024.2 | 232.51 | 1025.0 | 553.21 | 1025.2 | 2,713.73  |
| 1023.6 | 5.61    | 1024.4 | 233.73 | 1025.5 | 554.62 | 1025.5 | 21,666.27 |
| 1023.7 | 11.23   | 1024.6 | 234.95 | 1026.0 | 557.23 |        |           |
| 1023.8 | 3.45    | 1024.8 | 235.91 | 1026.5 | 572.20 |        |           |
| 1024.0 | 15.12   | 1025.0 | 236.45 | 1027.0 | 576.01 |        |           |
| 1024.2 | 24.52   | 1025.2 | 236.79 | 1027.5 | 578.65 |        |           |
| 1024.4 | 31.05   | 1025.4 | 236.95 | 1028.0 | 581.82 |        |           |
| 1024.6 | 21.81   | 1025.6 | 237.04 | 1028.5 | 584.47 |        |           |
| 1024.8 | 45.20   | 1025.8 | 237.14 | 1029.0 | 587.50 |        |           |
| 1025.0 | 52.55   | 1026.0 | 237.24 | 1029.5 | 590.10 |        |           |
| 1025.2 | 61.77   | 1026.2 | 237.23 | 1030.0 | 592.20 |        |           |
| 1025.4 | 69.11   | 1026.4 | 237.57 | 1030.5 | 594.35 |        |           |
| 1025.6 | 74.32   | 1026.6 | 237.67 | 1031.0 | 596.50 |        |           |
| 1025.8 | 83.44   | 1026.8 | 237.87 | 1031.5 | 598.65 |        |           |
| 1026.0 | 92.60   | 1027.0 | 238.44 | 1032.0 | 600.79 |        |           |
| 1026.2 | 104.82  | 1027.2 | 239.25 | 1032.5 | 602.95 |        |           |
| 1026.4 | 116.03  | 1027.4 | 239.45 | 1033.0 | 605.10 |        |           |
| 1026.6 | 127.21  | 1027.6 | 239.52 | 1033.5 | 607.20 |        |           |
| 1026.8 | 138.37  | 1027.8 | 239.52 | 1034.0 | 609.34 |        |           |
| 1027.0 | 149.58  | 1028.0 | 239.74 | 1034.5 | 611.48 |        |           |
| 1027.2 | 160.79  | 1028.2 | 239.74 | 1035.0 | 613.62 |        |           |
| 1027.4 | 172.00  | 1028.4 | 239.74 | 1035.5 | 615.76 |        |           |
| 1027.6 | 183.21  | 1028.6 | 239.74 | 1036.0 | 617.90 |        |           |
| 1027.8 | 194.42  | 1028.8 | 239.74 | 1036.5 | 620.04 |        |           |
| 1028.0 | 205.63  | 1029.0 | 239.74 | 1037.0 | 622.18 |        |           |
| 1028.2 | 216.84  | 1029.2 | 239.74 | 1037.5 | 624.32 |        |           |
| 1028.4 | 228.05  | 1029.4 | 239.74 | 1038.0 | 626.46 |        |           |
| 1028.6 | 239.26  | 1029.6 | 239.74 | 1038.5 | 628.60 |        |           |
| 1028.8 | 250.47  | 1029.8 | 239.74 | 1039.0 | 630.74 |        |           |
| 1029.0 | 261.68  | 1030.0 | 239.74 | 1039.5 | 632.88 |        |           |
| 1029.2 | 272.89  | 1030.2 | 239.74 | 1040.0 | 635.02 |        |           |
| 1029.4 | 284.10  | 1030.4 | 239.74 | 1040.5 | 637.16 |        |           |
| 1029.6 | 295.31  | 1030.6 | 239.74 | 1041.0 | 639.30 |        |           |
| 1029.8 | 306.52  | 1030.8 | 239.74 | 1041.5 | 641.44 |        |           |
| 1030.0 | 317.73  | 1031.0 | 239.74 | 1042.0 | 643.58 |        |           |
| 1030.2 | 328.94  | 1031.2 | 239.74 | 1042.5 | 645.72 |        |           |
| 1030.4 | 340.15  | 1031.4 | 239.74 | 1043.0 | 647.86 |        |           |
| 1030.6 | 351.36  | 1031.6 | 239.74 | 1043.5 | 650.00 |        |           |
| 1030.8 | 362.57  | 1031.8 | 239.74 | 1044.0 | 652.14 |        |           |
| 1031.0 | 373.78  | 1032.0 | 239.74 | 1044.5 | 654.28 |        |           |
| 1031.2 | 385.00  | 1032.2 | 239.74 | 1045.0 | 656.42 |        |           |
| 1031.4 | 396.21  | 1032.4 | 239.74 | 1045.5 | 658.56 |        |           |
| 1031.6 | 407.42  | 1032.6 | 239.74 | 1046.0 | 660.70 |        |           |
| 1031.8 | 418.63  | 1032.8 | 239.74 | 1046.5 | 662.84 |        |           |
| 1032.0 | 429.84  | 1033.0 | 239.74 | 1047.0 | 664.98 |        |           |
| 1032.2 | 441.05  | 1033.2 | 239.74 | 1047.5 | 667.12 |        |           |
| 1032.4 | 452.26  | 1033.4 | 239.74 | 1048.0 | 669.26 |        |           |
| 1032.6 | 463.47  | 1033.6 | 239.74 | 1048.5 | 671.40 |        |           |
| 1032.8 | 474.68  | 1033.8 | 239.74 | 1049.0 | 673.54 |        |           |
| 1033.0 | 485.89  | 1034.0 | 239.74 | 1049.5 | 675.68 |        |           |
| 1033.2 | 497.10  | 1034.2 | 239.74 | 1050.0 | 677.82 |        |           |
| 1033.4 | 508.31  | 1034.4 | 239.74 | 1050.5 | 679.96 |        |           |
| 1033.6 | 519.52  | 1034.6 | 239.74 | 1051.0 | 682.10 |        |           |
| 1033.8 | 530.73  | 1034.8 | 239.74 | 1051.5 | 684.24 |        |           |
| 1034.0 | 541.94  | 1035.0 | 239.74 | 1052.0 | 686.38 |        |           |
| 1034.2 | 553.15  | 1035.2 | 239.74 | 1052.5 | 688.52 |        |           |
| 1034.4 | 564.36  | 1035.4 | 239.74 | 1053.0 | 690.66 |        |           |
| 1034.6 | 575.57  | 1035.6 | 239.74 | 1053.5 | 692.80 |        |           |
| 1034.8 | 586.78  | 1035.8 | 239.74 | 1054.0 | 694.94 |        |           |
| 1035.0 | 597.99  | 1036.0 | 239.74 | 1054.5 | 697.08 |        |           |
| 1035.2 | 609.20  | 1036.2 | 239.74 | 1055.0 | 699.22 |        |           |
| 1035.4 | 620.41  | 1036.4 | 239.74 | 1055.5 | 701.36 |        |           |
| 1035.6 | 631.62  | 1036.6 | 239.74 | 1056.0 | 703.50 |        |           |
| 1035.8 | 642.83  | 1036.8 | 239.74 | 1056.5 | 705.64 |        |           |
| 1036.0 | 654.04  | 1037.0 | 239.74 | 1057.0 | 707.78 |        |           |
| 1036.2 | 665.25  | 1037.2 | 239.74 | 1057.5 | 709.92 |        |           |
| 1036.4 | 676.46  | 1037.4 | 239.74 | 1058.0 | 712.06 |        |           |
| 1036.6 | 687.67  | 1037.6 | 239.74 | 1058.5 | 714.20 |        |           |
| 1036.8 | 698.88  | 1037.8 | 239.74 | 1059.0 | 716.34 |        |           |
| 1037.0 | 710.09  | 1038.0 | 239.74 | 1059.5 | 718.48 |        |           |
| 1037.2 | 721.30  | 1038.2 | 239.74 | 1060.0 | 720.62 |        |           |
| 1037.4 | 732.51  | 1038.4 | 239.74 | 1060.5 | 722.76 |        |           |
| 1037.6 | 743.72  | 1038.6 | 239.74 | 1061.0 | 724.90 |        |           |
| 1037.8 | 754.93  | 1038.8 | 239.74 | 1061.5 | 727.04 |        |           |
| 1038.0 | 766.14  | 1039.0 | 239.74 | 1062.0 | 729.18 |        |           |
| 1038.2 | 777.35  | 1039.2 | 239.74 | 1062.5 | 731.32 |        |           |
| 1038.4 | 788.56  | 1039.4 | 239.74 | 1063.0 | 733.46 |        |           |
| 1038.6 | 799.77  | 1039.6 | 239.74 | 1063.5 | 735.60 |        |           |
| 1038.8 | 810.98  | 1039.8 | 239.74 | 1064.0 | 737.74 |        |           |
| 1039.0 | 822.19  | 1040.0 | 239.74 | 1064.5 | 739.88 |        |           |
| 1039.2 | 833.40  | 1040.2 | 239.74 | 1065.0 | 742.02 |        |           |
| 1039.4 | 844.61  | 1040.4 | 239.74 | 1065.5 | 744.16 |        |           |
| 1039.6 | 855.82  | 1040.6 | 239.74 | 1066.0 | 746.30 |        |           |
| 1039.8 | 867.03  | 1040.8 | 239.74 | 1066.5 | 748.44 |        |           |
| 1040.0 | 878.24  | 1041.0 | 239.74 | 1067.0 | 750.58 |        |           |
| 1040.2 | 889.45  | 1041.2 | 239.74 | 1067.5 | 752.72 |        |           |
| 1040.4 | 900.66  | 1041.4 | 239.74 | 1068.0 | 754.86 |        |           |
| 1040.6 | 911.87  | 1041.6 | 239.74 | 1068.5 | 757.00 |        |           |
| 1040.8 | 923.08  | 1041.8 | 239.74 | 1069.0 | 759.14 |        |           |
| 1041.0 | 934.29  | 1042.0 | 239.74 | 1069.5 | 761.28 |        |           |
| 1041.2 | 945.50  | 1042.2 | 239.74 | 1070.0 | 763.42 |        |           |
| 1041.4 | 956.71  | 1042.4 | 239.74 | 1070.5 | 765.56 |        |           |
| 1041.6 | 967.92  | 1042.6 | 239.74 | 1071.0 | 767.70 |        |           |
| 1041.8 | 979.13  | 1042.8 | 239.74 | 1071.5 | 769.84 |        |           |
| 1042.0 | 990.34  | 1043.0 | 239.74 | 1072.0 | 771.98 |        |           |
| 1042.2 | 1001.55 | 1043.2 | 239.74 | 1072.5 | 774.12 |        |           |
| 1042.4 | 1012.76 | 1043.4 | 239.74 | 1073.0 | 776.26 |        |           |
| 1042.6 | 1023.97 | 1043.6 | 239.74 | 1073.5 | 778.40 |        |           |
| 1042.8 | 1035.18 | 1043.8 | 239.74 | 1074.0 | 780.54 |        |           |
| 1043.0 | 1046.39 | 1044.0 | 239.74 | 1074.5 | 782.68 |        |           |
| 1043.2 | 1057.60 | 1044.2 | 239.74 | 1075.0 | 784.82 |        |           |
| 1043.4 | 1068.81 | 1044.4 | 239.74 | 1075.5 | 786.96 |        |           |
| 1043.6 | 1080.02 | 1044.6 | 239.74 | 1076.0 | 789.10 |        |           |
| 1043.8 | 1091.23 | 1044.8 | 239.74 | 1076.5 | 791.24 |        |           |
| 1044.0 | 1102.44 | 1045.0 | 239.74 | 1077.0 | 793.38 |        |           |
| 1044.2 | 1113.65 | 1045.2 | 239.74 | 1077.5 | 795.52 |        |           |
| 1044.4 | 1124.86 | 1045.4 | 239.74 | 1078.0 | 797.66 |        |           |
| 1044.6 | 1136.07 | 1045.6 | 239.74 | 1078.5 | 799.80 |        |           |
| 1044.8 | 1147.28 | 1045.8 | 239.74 | 1079.0 | 801.94 |        |           |
| 1045.0 | 1158.49 | 1046.0 | 239.74 | 1079.5 | 804.08 |        |           |
| 1045.2 | 1169.70 | 1046.2 | 239.74 | 1080.0 | 806.22 |        |           |
| 1045.4 | 1180.91 | 1046.4 | 239.74 | 1080.5 | 808.36 |        |           |
| 1045.6 | 1192.12 | 1046.6 | 239.74 | 1081.0 | 810.50 |        |           |
| 1045.8 | 1203.33 | 1046.8 | 239.74 | 1081.5 | 812.64 |        |           |
| 1046.0 | 1214.54 | 1047.0 | 239.74 | 1082.0 | 814.78 |        |           |
| 1046.2 | 1225.75 | 1047.2 | 239.74 | 1082.5 | 816.92 |        |           |
| 1046.4 | 1236.96 | 1047.4 | 239.74 | 1083.0 | 819.06 |        |           |
| 1046.6 | 1248.17 | 1047.6 | 239.74 | 1083.5 | 821.20 |        |           |
| 1046.8 | 1259.38 | 1047.8 | 239.74 | 1084.0 | 823.34 |        |           |
| 1047.0 | 1270.59 | 1048.0 | 239.74 | 1084.5 | 825.48 |        |           |
| 1047.2 | 1281.80 | 1048.2 | 239.74 | 1085.0 | 827.62 |        |           |
| 1047.4 | 1293.01 | 1048.4 | 239.74 | 1085.5 | 829.76 |        |           |
| 1047.6 | 1304.22 | 1048.6 | 239.74 | 1086.0 | 831.90 |        |           |
| 1047.8 | 1315.43 | 1048.8 | 239.74 | 1086.5 | 834.04 |        |           |
| 1048.0 | 1326.64 | 1049.0 | 239.74 | 1087.0 | 836.18 |        |           |
| 1048.2 | 1337.85 | 1049.2 | 239.74 | 1087.5 | 838.32 |        |           |
| 1048.4 | 1349.06 | 1049.4 | 239.74 | 1088.0 | 840.46 |        |           |
| 1048.6 | 1360.27 | 1049.6 | 239.74 | 1088.5 | 842.60 |        |           |
| 1048.8 | 1371.48 | 1049.8 | 239.74 | 1089.0 | 844.74 |        |           |
| 1049.0 | 1382.69 | 1050.0 | 239.74 | 1089.5 | 846.88 |        |           |
| 1049.2 | 1393.90 | 1050.2 | 239.74 | 1090.0 | 849.02 |        |           |
| 1049.4 | 1405.11 | 1050.4 | 239.74 | 1090.5 | 851.16 |        |           |
| 1049.6 | 1416.32 | 1050.6 | 239.74 | 1091.0 | 853.30 |        |           |
| 1049.8 | 1427.53 | 1050.8 | 239.74 | 1091.5 | 855.44 |        |           |
| 1050.0 | 1438.74 | 1051.0 | 239.74 | 1092.0 | 857.58 |        |           |
| 1050.2 | 1449.95 | 1051.2 | 239.74 | 1092.5 | 859.72 |        |           |
| 1050.4 | 1461.16 | 1051.4 | 239.74 | 1093.0 | 861.86 |        |           |
| 1050.6 | 1472.37 | 1051.6 | 239.74 | 1093.5 | 864.00 |        |           |
| 1050.8 | 1483.58 | 1051.8 | 239.74 | 1094.0 | 866.14 |        |           |
| 1051.0 | 1494.79 | 1052.0 | 239.74 | 1094.5 | 868.28 |        |           |
| 1051.2 | 1506.00 | 1052.2 | 239.74 | 1095.0 | 870.42 |        |           |
| 1051.4 | 1517.21 | 1052.4 | 239.74 | 1095.5 | 872.56 |        |           |
| 1051.6 | 1528.42 | 1052.6 | 239.74 | 1096.0 | 874.70 |        |           |
| 1051.8 | 1539.63 | 1052.8 | 239.74 | 1096.5 | 876.84 |        |           |
| 1052.0 | 1550.84 | 1053.0 | 239.74 | 1097.0 | 878.98 |        |           |

## HYDROGRAPH COMPUTATION

EASTERN SPILLWAY HYDROGRAPH

NH 684

SHEET  
33WATERSHED OR PROJECT BAKER RIVER STATE N.H.STRUCTURE SITE OR SUBAREA SITE ADR. AREA 16.04 SQ. MI.T<sub>c</sub> 3.72 HR.RUNOFF CONDITION NO. IIRUNOFF CURVE NO. 68 STORM DISTRIB. CURVE B HYDROGRAPH FAMILY NO. 3STORM DURATION 6 HR.RAINFALL: POINT 8.75 IN.AREAL 7.26 IN.Q 3.65 IN.COMPUTED T<sub>p</sub> 2.74 HR.T<sub>p</sub> 4.55 HR.(T<sub>p</sub> + T<sub>c</sub>): COMPUTED 1.66 USED 1.5 REVISED T<sub>p</sub> 3.03Q<sub>p</sub> =  $\frac{624 A}{REV. T_p} = \underline{2,562}$  CFS.Q<sub>90</sub> = 9,274 CFS.K(COLUMN) = (2/T<sub>p</sub>) REV. T<sub>p</sub>.Q(COLUMN) = (q<sub>c</sub>/4<sub>p</sub>) Q<sub>90</sub>.

| LINE NO. | t HOURS | q CFS   | LINE NO. | t HOURS                                   | q CFS          | LINE NO. | t HOURS | q CFS |
|----------|---------|---------|----------|---|----------------|----------|---------|-------|
| 1        | 0.00    | 0.00    | 21       | 17.57                                     | 18.55          | 41       |         |       |
| 2        | 0.88    | 259.67  | 22       | 18.45                                     | 9.27           | 42       |         |       |
| 3        | 1.76    | 1762.06 | 23       | 19.33                                     | 0.40           | 43       |         |       |
| 4        | 2.64    | 4173.30 | 24       |   |                | 44       |         |       |
| 5        | 3.5     | 6083.74 | 25       |   | 29 = 43,559.99 | 45       |         |       |
| 6        | 4.39    | 6807.12 | 26       |   |                | 46       |         |       |
| 7        | 5.27    | 6352.69 | 27       | Q = $\frac{45(39)}{645.7}$                |                | 47       |         |       |
| 8        | 6.15    | 5425.29 | 28       |   |                | 48       |         |       |
| 9        | 7.03    | 4126.93 | 29       | Q = $\frac{(0.88)(43,559.99)}{645(1.05)}$ |                | 49       |         |       |
| 10       | 7.91    | 3245.92 | 30       | Q = $\frac{38,332.792}{10,345,800.0}$     |                | 50       |         |       |
| 11       | 8.79    | 1845.53 | 31       |   |                | 51       |         |       |
| 12       | 9.67    | 1224.17 | 32       | Q = 3.705                                 |                | 52       |         |       |
| 13       | 10.54   | 825.39  | 33       | %Err = $\frac{3.705 - 3.62}{3.62}$        |                | 53       |         |       |
| 14       | 11.42   | 528.62  | 34       | %Err = 2.3%                               |                | 54       |         |       |
| 15       | 12.30   | 352.41  | 35       |   |                | 55       |         |       |
| 16       | 13.19   | 231.85  | 36       |   |                | 56       |         |       |
| 17       | 14.06   | 132.11  | 37       |   |                | 57       |         |       |
| 18       | 14.94   | 74.19   | 38       |   |                | 58       |         |       |
| 19       | 15.82   | 46.37   | 39       |   |                | 59       |         |       |
| 20       | 16.70   | 27.52   | 40       |   |                | 60       |         |       |

## HYDROGRAPH COMPUTATION

FREEWAY HOUSING

NH 684

WATERWIDE OR PROJECT RAVINE STATE N.H.STRUCTURE SITE OR SUBAREA SITE 5DRL AREA 16.04 SQ. MI.  $T_c$  1.72 HR. RUNOFF CONDITION NO. IIRUNOFF CURVE NO. 68 STORM DISTRIB. CURVE B HYDROGRAPH FAMILY NO. 2STORM DURATION 6 HR. RAINFALL: 0.587 POINT 17.5 IN. AREAL 0.83 (17.5) IN. $Q$  10.10 IN. COMPUTED  $T_p$  0.74 HR.  $T_o$  5.15 HR. $(T_o + T_p)$  COMPUTED 1.89 : USED 2.0 REVISED  $T_o$  2.58 $Q_p = \frac{CFA}{LUT_p} = 3009.05$  CFS.  $Q_{9p} = 35,391.40$  CFS. $Q(COLUMN) = (1/T_p) \text{ REV. } T_o$  $Q(COLUMN) = (9c/9_p) Q_{9p}$ 

| LINE NO. | t HOURS | Q CFS     | LINE NO. | t HOURS  | Q CFS      | LINE NO. | t HOURS | Q CFS |
|----------|---------|-----------|----------|--|------------|----------|---------|-------|
| 1        | 0       | 0.00      | 21       | 14.45  | 121.56     | 41       |         |       |
| 2        | 0.72    | 121.57    | 22       | 15.17  | 91.17      | 42       |         |       |
| 3        | 1.44    | 1215.66   | 23       | 15.89  | 60.78      | 43       |         |       |
| 4        | 2.17    | 5166.54   | 24       | 16.62  | 30.39      | 44       |         |       |
| 5        | 2.89    | 17,027.52 | 25       | 17.34  | 0.00       | 45       |         |       |
| 6        | 3.61    | 18,622.46 | 26       | 18.06  | 146,912.06 | 46       |         |       |
| 7        | 4.33    | 21,722.85 | 27       | $\Delta t = 0.72$                                |            | 47       |         |       |
| 8        | 5.06    | 20,574.98 | 28       |  |            | 48       |         |       |
| 9        | 5.78    | 17,401.67 | 29       | $Q = \frac{(\Delta t)(C_{19})}{64.571}$          |            | 49       |         |       |
| 10       | 6.50    | 14,204.74 | 30       |  |            | 50       |         |       |
| 11       | 7.22    | 12,264.13 | 31       | $Q = \frac{1857 \times 0.83}{12.34 \times 0.80}$ |            | 51       |         |       |
| 12       | 7.95    | 10,500.68 | 32       | $Q = 12.3$                                       |            | 52       |         |       |
| 13       | 8.67    | 8,415.16  | 33       |  |            | 53       |         |       |
| 14       | 9.39    | 6,474.21  | 34       | $\% \text{ Error} = \frac{10.2 - 10.10}{10.10}$  |            | 54       |         |       |
| 15       | 10.11   | 4,572.51  | 35       | $\% \text{ Error} = 1.0\%$                       |            | 55       |         |       |
| 16       | 10.84   | 2,857     | 36       |  |            | 56       |         |       |
| 17       |         | 227.1     | 37       |  |            | 57       |         |       |
| 18       | 11.56   | 87.6      | 38       |  |            | 58       |         |       |
| 19       | 12.28   | 18.17     | 39       |  |            | 59       |         |       |
| 20       | 12.99   | 1.1       | 40       |  |            | 60       |         |       |



BAKER RIVER DAM  
SITE 8



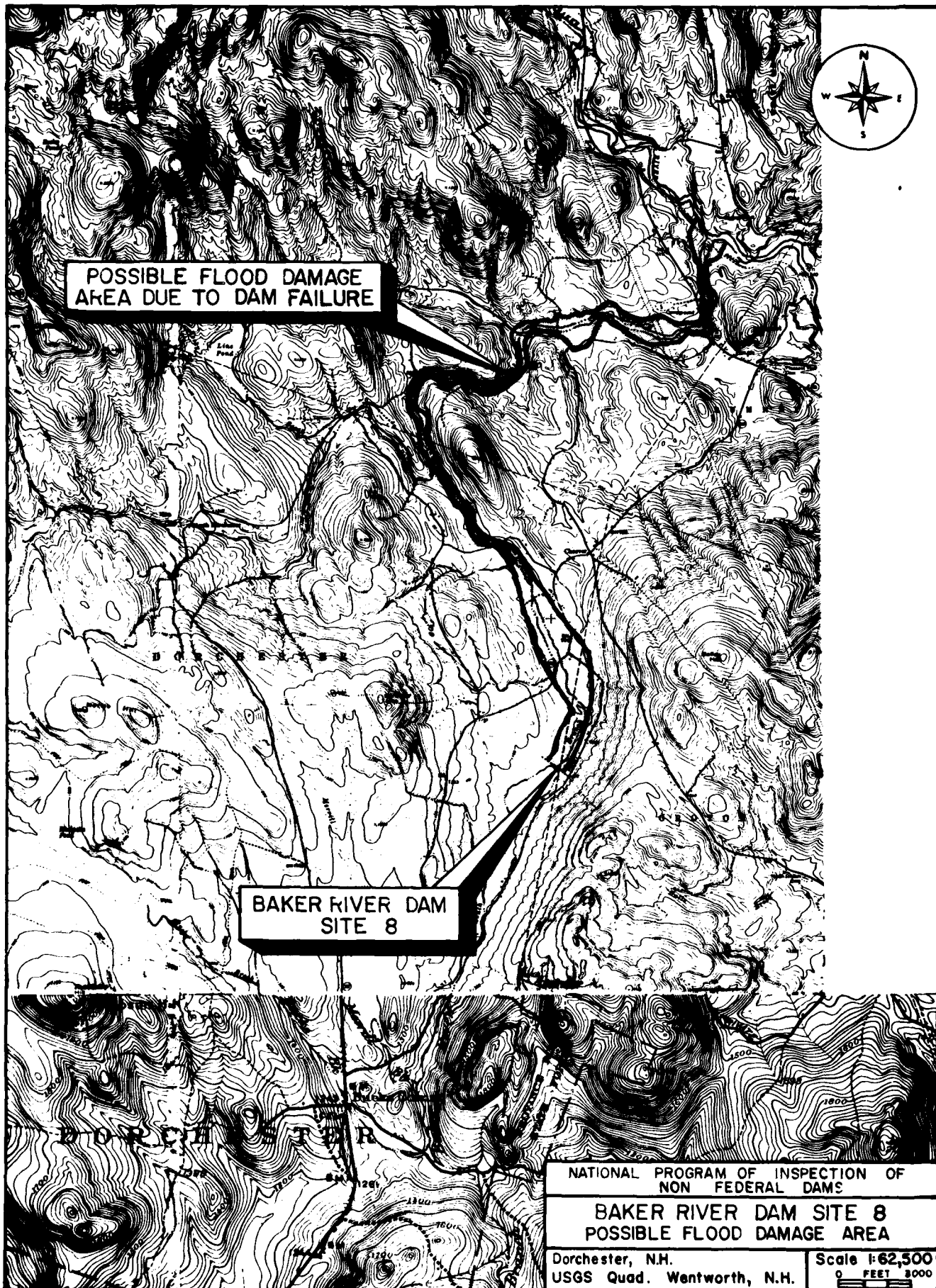
DRAINAGE AREA  
BOUNDARY

NATIONAL PROGRAM OF INSPECTION OF  
NON FEDERAL DAMS

BAKER RIVER DAM SITE 8  
DRAINAGE AREA

Dorchester, N.H.  
USGS Quad, Wentworth N.H.

Scale 1:62,500  
0 FEET 3000



POSSIBLE FLOOD DAMAGE  
AREA DUE TO DAM FAILURE

BAKER RIVER DAM  
SITE 8

|   |                               |
|---|-------------------------------|
| NATIONAL PROGRAM OF INSPECTION OF<br>NON FEDERAL DAMS |                               |
| BAKER RIVER DAM SITE 8<br>POSSIBLE FLOOD DAMAGE AREA  |                               |
| Dorchester, N.H.<br>USGS Quad. Wentworth, N.H.        | Scale 1:62,500<br>0 FEET 3000 |

APPENDIX E

INFORMATION AS CONTAINED IN  
THE NATIONAL INVENTORY OF DAMS

178 NED

# INVENTORY OF DAMS IN THE UNITED STATES

|       |                  |                 |                                   |             |
|-------|------------------|-----------------|-----------------------------------|-------------|
| STATE | INVENTORY NUMBER | CONTRACT NUMBER | CONTRACT DATE                     | REPORT DATE |
| NH    | 178              | NED             | 02                                | 18JUN79     |
| STATE | COUNTY           | CITY            | NAME                              | REPORT DATE |
| NH    | 009              | 02              | BAKER FLOODWATER RESERVOIR SITE B | 18JUN79     |

|                  |             |             |
|------------------|-------------|-------------|
| POPULAR NAME     | NAME OF DAM | REPORT DATE |
| SOUTH BRANCH DAM |             | 18JUN79     |
| POPULAR NAME     | NAME OF DAM | REPORT DATE |
| SOUTH BRANCH DAM |             | 18JUN79     |
| POPULAR NAME     | NAME OF DAM | REPORT DATE |
| SOUTH BRANCH DAM |             | 18JUN79     |

|             |                |          |                          |                          |                              |  |                    |            |
|-------------|----------------|----------|--------------------------|--------------------------|------------------------------|--|--------------------|------------|
| TYPE OF DAM | YEAR COMPLETED | PURPOSES | STORAGE CAPACITY (AC FT) | HYDROPOWER CAPACITY (KW) | IRREGULAR CAPACITIES (AC FT) | NEAREST DOWNSTREAM CITY - TOWN - VILLAGE | DIST FROM DAM (MI) | POPULATION |
| 01          | 1968           | C        | 71                       | 52                       | 4754                         |  | 0                  | 120        |

|         |
|---------|
| REMARKS |
|         |

|          |          |                         |                     |                     |           |          |             |            |            |             |
|----------|----------|-------------------------|---------------------|---------------------|-----------|----------|-------------|------------|------------|-------------|
| U.S. HAS | SPILLWAY | MAXIMUM DISCHARGE (CFS) | VOLUME OF DAM (CFS) | POWER CAPACITY (KW) | INSTALLED | PROPOSED | LENGTH (FT) | WIDTH (FT) | DEPTH (FT) | NOTED WIDTH |
| 1        | 1462     | U                       | 400                 | 16560               | 314219    |          |             |            |            |             |

|                        |                       |                   |
|------------------------|-----------------------|-------------------|
| OWNER                  | ENGINEERING BY        | CONSTRUCTION BY   |
| N H WATER RESOURCES BD | SOIL CONSERVATION SER | LANDERS + GRIFFIN |

|        |              |           |             |
|--------|--------------|-----------|-------------|
| DESIGN | CONSTRUCTION | OPERATION | MAINTENANCE |
| NONE   | NONE         | NONE      | NONE        |

|                                  |                 |                             |
|----------------------------------|-----------------|-----------------------------|
| INSPECTION BY                    | INSPECTION DATE | AUTHORITY FOR INSPECTION    |
| HOWARD NEEDLES TAMMEN BERGENDOFF | 17 MAY 79       | PUBLIC LAW 92-367 HAUG 1972 |

|         |
|---------|
| REMARKS |
|         |

DIST UNN FED R PHY/VED SCS A VER/DATE  
N N N : B 18JUN79

REPRODUCED AT GOVERNMENT EXPENSE

**END**

**FILMED**

**8-85**

**DTIC**